

Appendix A

Giles Model

The Giles model [1-2] is based on absorption and gain parameters that are proportional to the cross sections. The rate and propagation equations are solved by integrating the spectral evolution back and forth along the fiber until it converges.

The model uses the two-level approximation, which assumes that the lifetime of the pump level is much smaller than the lifetime of the metastable level:

$$N_i = N_1 + N_2 \quad (A1)$$

$$\frac{\partial N_2}{\partial t} = \sum_{k=1}^K I_k (N_1 \sigma_k^a - N_2 \sigma_k^e) - \frac{N_2}{\tau_2} \quad (A2)$$

where N_i = total ions density

N_i = ions density in i th level ($i = 1, 2$)

σ_k^a = absorption cross sections of the beam

σ_k^e = emission cross sections of the beam

I_k = intensity of the k th beam

τ_2 = combined radiative and non-radiative decay time from level 2 to level 1.

The evolution of the power in each pump and signal beam is given by:

$$\frac{\partial P_{s,k}}{\partial z} = u_k \int (N_2 \sigma_k^e - N_1 \sigma_k^a) I_k dA \quad (A3)$$

where $u_k = +1$ for propagation in the positive z direction

$= -1$ for propagation in the negative z direction

$dA = r dr d\phi$ is the cylindrical coordinate system

Integrating the equation over the transverse plane yields:

$$\frac{\partial P_s(z)}{\partial z} = u_s P_s(z) (\bar{N}_2 \Gamma_{s,2} \sigma_s^e - \bar{N}_1 \Gamma_{s,1} \sigma_s^a) \quad (A4)$$

where $A_{eff} = \int \frac{N_i(r, \phi, z) dA}{N_i(0)}$, effective area of the dopant ions

$$\Gamma_{s,i} = \frac{A_{eff} \int I_K(r, \phi, z) N_i(r, \phi, z) dA}{P_S(z) \int N_i(r, \phi, z) dA}, \text{ overlap integral or confinement factor}$$

The Giles model provides a full spectral solution. The propagation equations are integrated backs and forth along the fiber until the solution converges. For the Giles model, the propagation equations are rewritten in terms wavelength, λ , dependent absorption and emission coefficients:

$$\alpha(\lambda_K) = \Gamma(\lambda_K) \bar{N}_i \sigma_K^a(\lambda_K) \quad (A5)$$

$$g(\lambda_K) = \Gamma(\lambda_K) \bar{N}_i N_K^e(\lambda_K) \quad (A6)$$

$$\frac{\partial P_K(z)}{\partial z} = u_S P_S(z) (N_2 \alpha_K - N_1 g_K) \quad (A7)$$

Steady-state solution to the rate equation gives the average population inversion along the fiber:

$$N_2(z) = \frac{\frac{\tau_2}{A_{eff}} \sum \frac{P_K \alpha_K}{h \gamma_K}}{1 + \sum \frac{P_K}{P_K^{IS}}} \quad (A8)$$

where the intrinsic saturation power is given by:

$$P_K^{IS} = \frac{h \gamma A_{eff}}{\Gamma_{K,2} \tau_2 (\sigma_K^a + \sigma_K^e)}$$

References

- [1] OptiAmplifier Manual
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Appendix B

Theory of Regenerative Amplifier

The theory of regenerative amplifier derived here is basically based on the linear configuration developed R. Loudon et. al. [1]. The theory is also valid for ring configurations since interference effects were not taken into account. A similar result is also obtained in [2] and [3].

The intensity damping rates associated with the two couplers are given by

$$\gamma_1 = \frac{cT_1}{p} \quad \text{and} \quad \gamma_2 = \frac{cT_2}{p} \quad (\text{B1})$$

where T_1 and T_2 are the transmittance of couplers C_1 and C_2 , respectively (see Fig. 6.1) and p is the perimeter of the cavity. The total damping rate of the cavity field is then determined by

$$\gamma_c = \frac{1}{2}(\gamma_1 + \gamma_2) \quad (\text{B2})$$

Applying an external signal of complex field E_{in} then excites the cavity field E , giving the output field, from coupler C_2 as

$$E_{out} = \sqrt{\gamma_1} E \quad (\text{B3})$$

The equation of motion for the cavity field E , atomic population inversion D and dipole moment d are described by the Maxwell-Bloch equation

$$\dot{E} + (\gamma_c + i\omega)E = g d + \sqrt{\gamma_2} E_{in} \quad (\text{B4})$$

$$\dot{D} + \gamma_{||} D = \gamma_{||} D_p - g(E^* d + E d^*) \quad (\text{B5})$$

$$\dot{d} + (\gamma_{\perp} + i\omega)d = g E D \quad (\text{B6})$$

Above the oscillating threshold, it is assumed that laser action occurs for a single mode of frequency w_L in resonance with the atomic transition. In the erbium-doped fiber lasers, the dipole moment decay rate γ_1 is much larger than the population inversion decay rate ($\gamma_1 \gg \gamma_i \approx \gamma_c$). Therefore, they are treated as class B lasers [4]. The laser pump is expressed in terms of the mean population inversion D_p that would be obtained in the absence of any cavity field, while coupling constant, g in Eq. (B4)-(B6) is from the interaction of the collective atomic dipole moment and cavity field.

Below threshold, there is only a single-frequency component in the cavity determined by the frequency of the input signal-frequency component in the input signal w_s . Thus, the input signal field takes the form

$$E_m = \varepsilon_m \exp(-i w_s t) = \varepsilon_m \exp[-i(w_L + \Delta w)t] \quad (B7)$$

where $\Delta w = w_s - w_L$ represents the amount of detuning and ε_m is the amplitude of input signal.

Below threshold, there is no mean excitation of the image-frequency field and no modulation of the population inversion and the dipole moment in the cavity is just contributed from the input signal. Then, we have

$$E = E_s \exp[-i(w_L + \Delta w)t] \quad (B8)$$

$$d = d_s \exp[-i(w_L + \Delta w)t] \quad (B9)$$

$$D = D_p \quad (B10)$$

Thus, Eq. (B4) and (B6) reduce to

$$(\gamma_c + i w) E_s = g d_s + \sqrt{\gamma_2} \varepsilon_m \quad (B11)$$

$$\gamma_1 d_s = g E_s D_p \quad (B12)$$

Substituting Eq. (B12) into (B11) gives the solution

$$E_s = \frac{\sqrt{\gamma_2} \varepsilon_{in}}{\gamma_c(1-C) + i\Delta w} \quad (\text{B13})$$

where $C = g^2 D_p / \gamma_c \gamma_L < 1$ below threshold.

The intensity gain is then given by

$$G(\Delta w) = \left(\frac{E_{out}}{\varepsilon_{in}} \right)^2 = \frac{\gamma_1 \gamma_2}{\Delta w^2 + \gamma_c^2 (1-C)^2} \quad (\text{B14})$$

From Eq. (B14), it is seen that the maximum gain achieved at zero detuning $\Delta w = 0$.

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Appendix C

Injection Locking Theory Based on Adler's Model

A standard method used to describe the injection locking phenomena is based on Adler's model [1]. This model explains very well the phenomena in the locking range. However, outside this locking range, there is no steady-state solution for the cavity phase, resulting in the limitation of the model [2].

In Adler's model, the eigenfield of the slave laser is given by

$$E_0(t) = \varepsilon_0(t) e^{j[w_0(t) + \phi_0(t)]} \quad (C1)$$

The injected signal from the master laser has the field in the same form

$$E_1(t) = \varepsilon_1(t) e^{j[w_1(t) + \phi_1(t)]} \quad (C2)$$

$\varepsilon_{0,1}(t)$ and $w_{0,1}$ represent the amplitude and angular frequency of the field of the slave laser and incident signal, respectively. Both the waves depend also on the phase $\phi_{0,1}(t)$.

Equations of time-evolution amplitude $\varepsilon_{0,1}(t)$ of the cavity signal are

$$\frac{d\varepsilon_0(t)}{dt} + \frac{(\gamma_e - \gamma_m)}{2} \varepsilon_0(t) = \gamma_e \varepsilon_1(t) \cos[\phi_0(t) - \phi_0(t)] \quad (C3)$$

$$\frac{d\phi_1(t)}{dt} + (w_1 - w_0) = -\frac{\gamma_e \varepsilon_1(t)}{\varepsilon_0(t)} \sin[\phi_0(t) - \phi_1(t)] \quad (C4)$$

where γ_e : cavity decay rate

γ_m : laser growth rate

γ_e : external decay rate

Solving phase equation (C4) under steady-state condition gives

$$(w_1 - w_0) = -\frac{\gamma_e \varepsilon_1}{\varepsilon_0} \sin[\phi_0 - \phi_1] \quad (C5)$$

But
$$-1 \leq \left\{ \sin[\phi_0 - \phi_1] \equiv \frac{(w_1 - w_0) \varepsilon_0}{\gamma_e \varepsilon_1} \right\} \leq 1$$

or
$$-\frac{\gamma_e \varepsilon_0}{\varepsilon_1} \leq w_1 - w_0 \leq \frac{\gamma_e \varepsilon_0}{\varepsilon_1}$$

The full locking range centered at resonance atomic transition frequency w_0 is then given by

$$\Delta w = 2\gamma_e \sqrt{I_1/I_0} \quad (C6)$$

where $I_{0,1} \propto \varepsilon_{0,1}^2$.

The round-trip power decrease due to external coupling can be related to coupler reflectivity by

$$R = e^{-\gamma_e \tau} \quad (C7)$$

where $\tau = nl/c$, round-trip time in the cavity length of l and refractive index of n .

This gives the external decay rate

$$\gamma_e = \frac{c}{l} \ln\left(\frac{1}{R}\right) \quad (C8)$$

Substituting equation (C8) into (C6) and use the relation of $w = 2\pi\nu$, gives the full locking range

$$\Delta\nu = \frac{c \ln\left(\frac{1}{R}\right)}{\pi l} \sqrt{P_1/P_0} \quad (C9)$$

where the power ratio, P_1/P_0 , is equivalence to I_1/I_0 .

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Appendix D

Publication List

International Journals

1. T. C. Teyo, M. K. Leong and H. Ahmad, "*Power Conversion Efficiency of Erbium doped Fibre Amplifiers With Optical Feedback*," accepted to be published in **J. Opt. Comm.**
2. T. C. Teyo, N. S. Mohd. Shah and H. Ahmad, "*Injection locking of erbium-doped fiber laser-amplifier*," **Microwave & Opt. Technol. Lett** , Vol. 36, No. 2, pp. 89-91, 2003.
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1. T. C. Teyo, M. K. Leong, N. S. Mohd. Shah, P. Poopalan, S. W. Harun and H. Ahmad, "*Characterization of EDFA using Different Measurement Methods*," submitted to **Malaysian Journal of Science**.

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4. T. C. Teyo, N. S. Mohd. Shah and H. Ahmad, '*Lasing Threshold In Gain-Clamped Erbium-Doped Fiber Amplifier*,' submitted to **J. Solid State Sc. and Technol.**
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