

4.1 Preliminary Processing

The oil palm leaflets, typical of monocotyledonous plants, comprise a mass of discrete vascular bundles embedded in parenchymatous tissue. It is this fibrous vascular tissue free from the embedding parenchymatous matter that provides the cellulosic fibres for pulp.

The parenchymatous matter is susceptible to fungal attack. In the early stage, the fungus attacks the food content of the parenchyma cells. The cell walls were not attacked but this could not be ruled out on prolonged exposure (Khoo, 1989).

Due to this, the leaflets were immediately cut up upon arrival and air-dried, then kept in sealed plastic bags to be stored indefinitely.

4.2 Density

The mean density of the midrib was 0.547 g/cc while that of the leaf blade was 0.241 g/cc. This is shown in Table 7. The generally low density values could be related to thin cell walls and it also indicates that shorter cooking times might be sufficient for the cooking liquor to penetrate the fibre strands (Yusoff *et al.*, 1984).

Chemical analysis

The results of the proximate chemical composition of oil palm midrib and leafblade are given in Table 11. Comparing the data with those reported by Khan and Peh (1) for Malaysian hardwoods, it is clear that the values for the midrib are typical of Malaysian hardwoods except for their pentosans content. In comparison with some non-woody species, the oil palm midrib contained lower lignin and pentosans contents (10.7% and 25.3% respectively), but a higher lignin content (24.5%) and comparable with grasses than to grasses or straws as shown in Table 10.

However, the very high ash, high alkali, alcohol-insoluble and hot water solubilities and low alpha-cellulose content of the leaf blade as compared to the midrib, render it unfavourable for papermaking. The very high ash (9.1%), alkali affect the economy of any recovery process connected with pulping. The low alpha-cellulose content (24.1%), high alkali solubility (51%) and high lignin content (30.3%) all indicate a heavy chemical consumption combined with a low pulp yield. All of these expectations were frequently confirmed from this study.

2.1 Morphological characteristics

Table 3 presents a comparison of the morphology of fibre from the different parts of the oil palm.

The similarity of the oil palm midrib fibre to low density hardwoods is in having rather short length and relatively thin walls. The midrib with thinner walls has the potential as a pulping material since thin cell walls are indicative of better general paper making properties. Pulp made from thin-walled fibres are expected to be dense and well formed whereas those derived from thick-walled fibres are generally bulky with coarse surfaces. Thick-walled fibres also adversely influence bursting strength, tensile strength and folding endurance (Peh *et al.*, 1986).

The thin walled fibres of the midrib, with large lumen, and a moderate coefficient of suppleness and based on the criteria of Istas *et al.* (1964), such fibres are expected to not actually collapse (flatten), giving an elliptical cross-sectional form, producing good surface contact between adjacent fibres and hence good fibre to fibre bonding. The low Runkel ratio at 0.38 and moderate coefficient of suppleness (72.0%) of the midrib would be expected to confer storage strength properties to pulps produced from it. However, the high Runkel ratio (1.4) and low coefficient of suppleness (41.4%) would not favour pulping of the sheath blade. The high Runkel ratio indicates that the fibres are fairly thick-walled while the coefficient of suppleness

create not only thick walls but also a rather narrow lumen. The fibres are expected to show only a small amount of flattening in papermaking, which in turn gives a fairly poor surface contact and fairly poor fibre to fibre bonding.

From the microscopic studies, the fibres of both the midrib and leaf blade appeared as cylindrical cells with fine-pointed and gradually tapering ends. This can be seen in Plates 3 and 4. The length of the midrib fibre (1.72 mm) is about twice that of the leaf blade (0.89 mm). The diameter of the midrib fibre at 15.6 μ is larger than the diameter of the leaf blade fibre (11.1 μ). The lumen of the leaf blade (4.6 mm) is narrower compared to that of the midrib (11.2 mm) while the cell walls of the midrib (2.2 mm) are thinner than the cell walls of the leaf blade (3.2 mm). There was a large amount of non-fibrous matter present, mostly consisting of vessel elements and parenchymatous cells especially in the leaf blades.

Since the midribs contain most of the fibres suitable for papermaking while the leaf blades consist of shorter and broken fibres and a greater proportion of non-fibrous tissue, it is reasonable to expect the leaflets if cooked whole, to give pulps of lower yield and strength characteristics.

Pulping trials were conducted to determine the required conditions for achieving satisfactory results. A higher liquor to material ratio was needed to pulp the leaf blades of the leaves (whole) than the midrib on account of the waxy nature of the leaf blades.

When the leaves (whole) were pulped by the soda process, the non-fibrous matter dissolved, giving a poor yield (9.3%) of pulp. This can be seen in Table 12. Handsheets were not made since the yield was very low. Similarly, when the leaf blades were pulped by the soda process, a low yield (9.9%) was obtained as in Table 13.

Soda pulping

Table 14 shows the results of the pulping trials of the midrib by the soda process. It is apparent that the midrib is not easily pulped by this process even up to an active alkali (A.A.) of 18%.

Cooking below 17% A.A. was unfeasible as the low chemical concentrations were not sufficient to complete the digestion and adequately delignify the material as shown by the high kappa numbers. This resulted in the hard pulps, low yields and high amount of rejects. This is also true of the leaf blades as can be seen in Table 13. Since the yield was very poor, handsheets could not be made from the soda pulp of the leaf blades.

4.2 Sulphate pulping

It is clear from Table 15 that the midrib could be pulped by the sulphate process. An A.A. of not more than 18% was sufficient to produce a pulp with a kappa number of 21.4. Cooking below 18% A.A. did not significantly affect the yield but an A.A. below 15% was not feasible due to a low degree of digestion at that chemical concentration as shown by the high kappa numbers. A low yield (9.9%) was obtained when the leaf blades were pulped by the sulphate process as shown in Table 16. Only a set of handsheets could be made.

Table 17 gives the details of bleaching of the pulp obtained from Cook 4 with a kappa number of 21.4. A yield of 93% was obtained from the simple three stage (CEH) bleaching. There was an appreciable loss in yield of 8%.

4.3 NSSC pulping

Due to the bulky nature of the midrib, the liquor to wood ratio was kept at 7:1 to ensure better liquor circulation in the digester. The results of the NSSC pulping properties are given in Table 18.

As expected, there was a general reduction in total pulp yield and a decrease in Kappa number with increasing chemical concentration as shown in Figure 29. The material was not difficult to pulp as a chemical charge as low as 4%

produced an acceptable pulp yield (60.7%), but it was necessary to increase the sodium sulphite concentration beyond 12% since the Kappa number (117) remained high at that concentration (12%). However, even with a chemical charge of 16%, the Kappa number at 109 did not decrease much despite a large drop in yield to 52%. Considering the low yield and small improvement in Kappa number, it might not be worthwhile to pulp beyond 8% sodium sulphite concentration. The concentration of sodium carbonate was kept at 6% to provide a non-acidic pH. This did not prove to be adequate to cook 10 when the low concentration of sodium sulphite used (4%) could not provide the additional buffering action against the acids produced. Increasing the concentration of sodium carbonate to 8% could raise the pH to a more desirable level.

2.8 Pulp evaluation

Sulphate pulps

The results of the evaluation of the bleached and unbleached sulphate pulps are shown in Table 19. Their strength results are graphically presented in Figures 1 to 10.

A preliminary pulping trial of the leaf blades using an A.A. of 18% gave a very poor yield, hence only a set of handsheets were made. Since not only a set of

handsheets could be made, graphical evaluation could not be produced. However, comparing the results with those of the sulphate pulp of the midrib at the same A.A. of 18% and beating, it can be seen that the values for the leaf blades are lower than that of the midrib.

Evaluation of the unbleached sulphate pulps of the midrib showed the pulps to have quite similar properties except in the tearing strength where Cook 4 with the lowest kappa number gave the best results. In fact, Cook 4 showed the best development of strength on beating. When this pulp was bleached, however, an overall drop in strength was clearly noted.

Nevertheless, an unusual feature about this bleached pulp is that on beating, while the tearing strength remained practically constant, other strength values improved. Examination of the fibres showed that beating caused some changes to the cell wall structure but not much to the fibre length, thus explaining for the mild drop in tearing strength of the beaten pulps. This is especially so for the bleached pulp. Thus it could be inferred that these fibres were not easily shortened although the cell wall could be altered by beating. This is illustrated in Photomicrographs 5 to 9. In the bleached pulps, the tearing strength was retained down to a freeness value of 190 ml Csf, indicating little loss of fibre length.

4.9 Soda pulps

Results of the evaluation of the soda pulps are shown in Tables 20 and their strength results are depicted graphically in Figures 11 to 19.

With respect to the tearing strength of the soda pulps, the raw Cooks 6 and 7, especially the former which had the lowest kappa number, gave the poorest values. With low beating, Cook 8 had lower tearing strength than Cook 9, but on further beating at freeness less than 400 ml Csf, the tear improved and surpassed that of cook 9. Differences in other strength properties between the soda pulps were not so marked especially on beating as shown in Figures 12 to 19.

4.10 NSSC pulps

The full details of the NSSC pulp evaluation are given in Table 21. The strength properties are illustrated in Figures 20 to 28.

The NSSC pulp with the overall maximum strength, especially in tensile and bursting strength came from cook 13 (at 16% sodium sulphite) with a Kappa number of 109.

Cook 12 (at 12% sodium sulphite) showed a high tearing and bursting strength initially which dropped

rapidly on beating. Cook 10 (at 4% sodium sulphite) and cook 11 (at 8% sodium sulphite) were not easy to beat as the freeness dropped to only 280 ml Csf even after 90 minutes of beating. Cooks 10 and 11 showed a slight increase in overall strength properties on beating with the exception of tearing strength.

Insufficient chemical charge could be a reason for inadequate dispersion of the fibre bundles which led to the low strength properties of cook 10 and 11 (4% and 8% sodium sulphite respectively).

Cook 13 (16% sodium sulphite) was the easiest to beat with a rapid development for all strength properties except for a slight drop in tear. Strength development on beating was fast whereby after an hour of beating, the freeness dropped to 200 ml Csf. In fact, strength development was already noticeable after the first beating point.

Generally, the strength properties of the NSSC pulps from cooks 10 to 13 indicate a general improvement accompanied by a drop in Kappa number with increase of chemical charge. However, the strength improvement at more than a chemical charge of 12% might not be sufficient to offset the additional expenditure of chemicals and the reduced pulp yields. Cook 10, at

a low chemical charge of 4% and an average yield of 60.7% could be preferable to the other cooks.

From Figures 9 and 19, it can be seen that the freeness of the soda and sulphate pulps decreases as heating increases. The freeness of the NSSC pulps also dropped on heating but no clear trend was seen.

Prolonged heating causes the cellulosic fibre wall to gradually break up into extremely minute fibrils. It is this fibril formation that increases the retention of water (Technical Section of the British Paper and Board Makers' Association, 1949). Plates 5 to 9 illustrate this.

4.11 Comparison with sulphate pulps from oil palm trunk and empty fruit bunches (EFB)

From the work of Peh et al. (1976) and Ehee and Lee (1985), it was found that pulping of the trunk and EFB required prior to separation of the fibrous strands from the parenchymatous tissue. The operation, although time-consuming and requiring the use of auxiliary equipment was necessary not only to prevent biological degradation but also to produce cleaner and stronger pulps at a lower consumption of chemicals. The trunk was less messy to handle compared to the EFB which had a faster rate of deterioration.

Sulphate pulping of the EFB required higher chemical concentrations than the trunk, although the yields of the paper were generally better. An A.A. of 16% was needed to produce bleachable pulps for the EFB, whereas an A.A. of 14% was sufficient to produce pulps of bleachable grades for the trunk. On bleaching, the loss in yield for both materials was (9.3%), trunk (9.7%) was almost similar but the EFB gave a brighter pulp (90%) compared to the trunk (67%).

Higher chemical concentrations were needed to produce sulphate pulps of the midrib compared to both the trunk and EFB probably due to the higher lignin content in the midrib. Yields were generally lower, but on bleaching, the yield was higher for the midrib than both the trunk and EFB and the brightness was better than the trunk but lower compared to EFB.

The sulphate pulp from the trunk was easier to beat with a faster development of strength which was generally better, especially in folding endurance to that of the corresponding pulp from the EFB. The only redeeming feature of the latter was in having very good stretching property.

The sulphate pulp from the midrib was also easy to beat with a fast development of strength. Although the tensile index and folding endurance were better than that of the trunk, tearing strength and stretch of the midrib were far better than the trunk.

Compared to the EFB, the sulphate pulp of the midrib is better in terms of tear and tensile index but the stretch was superior in the EFB.

12 Comparison with NSSC pulps from oil palm trunk

From studies conducted by Yuseff (1985), it was found that the fibrous strands from the oil palm trunks were suitable material for producing NSSC pulps of acceptable strength properties at low chemical charges of 4 to 10% sodium sulphite and at short digestion times. Moderate pulp yields of 62 to 70% were obtained. Excessive addition of sodium carbonate, up to 12% was required to achieve the non-alkaline condition in the cooking liquor.

The results also suggested that to achieve a kappa number of over 70, the amount of sodium sulphite used during digestion should not be more than 6%. Apart from tearing strength, the pulps possessed good overall strength properties. Beating of the NSSC pulp gave rise to a fast development of strength properties, resulting in a high degree of inter-fibre bonding.

NSSC pulping of the midrib required higher chemical charges (4-16%) to produce moderate yields (52-60.7%) compared to the low chemical charges (4-10%) for the trunk to produce higher yields of between 62-70%. Perhaps the

ference in cooking temperature (170°C for the trunk, 160°C for the midrib) affected the yields.

A chemical charge of up to 16% could only produce pulp kappa number 109, whereas for the trunk, 6% sodium sulphite was sufficient to produce a kappa number of above 100. Strength properties were generally better for the trunk than in the midrib.

13. Comparison with pulps from oil palm petiole

From studies conducted by Joedidobroto (1982), it was found that the chemical pulps from oil palm petiole had good properties.

Prior removal of the parenchyma tissues was necessary to produce high yields of pulps. Pulping by the soda process produced pulps with a rather high kappa number (60) and high screenings. Delignification was improved by the addition of a small amount of anthraquinone (0.15%). The strength properties of the pulps were comparable to those of pine sulphate pulps obtained from cooks at similar active charge (14% and sulphidity of 20%).

The strength properties of the pulps were quite similar to those of pine sulphate pulp except for the low burst values. The pulps gave breaking lengths close to 10 km, which is rather high and similar to softwood pulps. The soda process produced the weakest pulps. The paper strength

properties of the petiole pulp could probably be compared with hardwood sulphate pulp.

From the morphological point of view, the length of the midrib fibre (1.82 ± 0.55 mm) was not much different from that of the petiole [1.58 mm (periphery), 1.35 mm (inner part)]. The felting power of the peripheral fibres was 138 while that of the inner fibres was 91. The felting power of the midrib fibre was 116.3. However, the Kunkel ratio of the midrib fibre at 0.39 was much smaller than both the peripheral fibres (2.41) and the inner fibres (0.43). This feature could render the midrib more favourable in papermaking.

However, the chemical composition of the petiole was more favourable than the midrib in terms of pulping. The lower lignin content (24.5%) and alcohol-benzene solubility (2.5%) of the midrib would indicate a higher chemical consumption combined with a lower yield compared to the petiole (18.8%, 6.5% respectively). This was evident in the soda and pulping of the materials. Soda pulping of the petiole at 14% A.A. produced considerably more yield (48.9%) combined with a lower Kappa number (24.0) than the soda pulping of the midrib at the same A.A. [yield (28.7%), Kappa number (105.7)]. To achieve a Kappa number of around 24, only 14% A.A. in the sulphate pulping of the petiole whereas 18% A.A. was needed to pulp the midrib.

The tensile strength of the pulp made of the stems is comparable to the petiole while that of the bleached and bleached sulphate pulps of the stems were superior to bleached sulphate pulps of the similar material, even as the petiole pulps whereas the yield and NDFC of the stems were weaker. The average length of the stem pulps were longest as compared to that of the pulps of the stems.

Comparison with other nonwoody fibres

Studies by Clark and Bagby (1977) have shown that a new plant i.e. kenaf (*Hibiscus sabdariffa*) has potential in papermaking. The average fibre length of the kenaf woody fractions is 1.18 cm. The alpha-cellulose content of kenaf at 16.5% is comparable to spruce (softwood) while its lignin content (17.3%) is appreciably lower than both spruce (27.6%) and maple

The stalks either green or field-dried could be directly processed into sulphate pulps of high quality.

An A.A. of 16 - 16.5% was needed to produce bleachable pulp. Strength characteristics of kenaf pulp were similar at the same freeness level to those of commercial softwood pulps and except for resistance to tear comparable to softwood pulps (Clark and Bagby 1977).

The bleached pulps were also blended with commercial wood pulps to produce bond papers. Bond papers containing 16% kenaf, 20% hardwood and 23% softwood pulps had good burst factor, breaking length and folding endurance but a somewhat lower tear factor than those containing 67% softwood and 33% hardwood pulp in the furnish (Clark and Bagby, 1970).

The oil palm midrib contains a higher content of alpha-cellulose compared to kenaf (36%) while the pentosans content of both materials are comparable. The lignin content of the midrib at 24.5% is slightly higher than kenaf (17.5%) possibly explaining the slightly higher A.A. (18%) required for producing bleachable pulps of the midrib.

The tearing strength of the bleached sulphate pulp of the midrib is comparable to that of the bond paper to which 40% kenaf had been added. The beating length of the bond paper was rather similar to that of the midrib pulp.

(where 24 g of OD pulp are needed for a set of 12 handsheets)

Calculations related to pulping are FRIM's adaptations of those found in Pulp and Paper Science and Technology Vol. 1 Pulp (Libby, 1962),

(a) Kappa number of pulp

	1	2
Wt. of beaker (g)	42.8467	52.8722
Wt. of beaker + AD pulp (g)	48.2792	58.1705
Wt. of AD pulp (g) [A]	5.4325	5.2983
(B = OD content of pulp = 37.2574)		
W = wt. of OD pulp = B/100 x A (g)	2.0240	1.9740

Calculation of Kappa number for 1

n = normality of thiosulphate solution = 0.2N

b = vol. of thiosulphate solution consumed in the blank determination = 49.8 ml

a = vol. of thiosulphate consumed in test = 27.65 ml

p = vol. of permanganate consumed

f = factor for correction to 50% permanganate consumption (dependent on the value of p)

k = Kappa number

$$p = (b - a)n/0.1$$
$$= (49.8 - 27.65)0.2/0.1$$
$$= 44.3$$

$$k = p \times f/W$$