OPTIMIZATION OF AIN/GaN STRAINED-LAYER SUPERLATTICE FOR GaN EPITAXY ON Si(111) SUBSTRATE

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OPTIMIZATION OF AIN/GaN STRAINED-LAYER SUPERLATTICE FOR GaN EPITAXY ON Si(111) SUBSTRATE

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OPTIMIZATION OF AIN/GaN STRAINED-LAYER SUPERLATTICE FOR GaN EPITAXY ON Si(111) SUBSTRATE

ABSTRACT

Most works involving GaN technology on Si (111) substrate, especially for device applications suffer from high density dislocations and cracks in the sample which reduces the performance of the devices. The objective of this study is to introduce aluminium nitride/gallium nitride (AlN/GaN) strained-layer superlattice (SLS) structure to avoid abrupt changes in thermal expansion coefficient between epilayer and Si substrate. In addition, this structure reduces the propagation of threading dislocation inside the sample. Indirectly, the structure will reduce the bowing effect on the sample. The growth was performed by introducing nitridation surface treatment (NST) just before depositing high temperature AIN nucleation layer at 1000 °C for different nitridation time of 40,220 and 400 s. Subsequently, AlN/GaN SLS layer of 11 and 13 nm respective thickness with different number of pairs of 20, 40, 60 and 80 pair was grown on top of the AIN nucleation layer. Undoped GaN with thickness of 500 nm was eventually grown on the SLS structure at temperature of 1125 °C to investigate the sustainability of AlN/GaN SLS to avoid cracks on the sample. Although bowing results from X-ray rocking curve (XRC) analysis display optimum, lowest full width half maximum (FWHM) for 60 SLS pairs which suggest a reduction in dislocation with an increase in number of SLS pair. Cross section images of field effect scanning electron microscopy (FESEM) shows fine and abrupt SLS pair structure while surface analysis shows smoother surface with increment in number of SLS pair. Roughness analysis conducted using atomic force microscopy (AFM) correlates well with both XRC results and FESEM surface results. Investigation of bowing effects also provides positive results in which there is an optimum bowing parameters which is required to produce crack-free GaN on Si (111). In conclusion, 60

pairs of AlN/GaN strained-layer superlattice can successfully sustain 1 μ m undoped GaN, thus, producing crack-free GaN layer on Si (111) substrate.

Keywords: GaN on Si (111), MOCVD, crack-free, SLS

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OPTIMISASI LAPISAN MENEGANG SUPER KEKISI AIN/GaN UNTUK EPITAKSI GaN DI ATAS SUBSTRAT Si(111)

ABSTRAK

Kebanyakan kerja melibatkan teknologi GaN di atas substrat silikon (111), terutamanya untuk aplikasi alatan mengalami ketumpatan dislokasi yang tinggi dan keretakan di dalam sampel yang mengurangkan prestasi alatan yang dicambah di atas substrat silikon (111). Objektif kajian ini adalah untuk memperkenalkan struktur aluminium nitrida/gallium nitrida (AlN/GaN) lapisan menegang super kekisi (SLS) untuk mencegah perubahan mengejut pada pekali pengembangan terma antara lapisan epi dan substrat silikon. Tambahan pula, struktur ini mengurangkan penyebaran bebenang dislokasi di dalam sampel. Secara tidak langsung, struktur ini akan mengurangkan kesan melengkung di atas sampel. Percambahan dilakukan dengan memercikkan lapisan penukleusan AlN suhu tinggi pada 1000 °C. Seterusnya, AlN/GaN SLS masing-masing pada ketebalan 10 dan 15 nm dengan bilangan pasangan yang berbeza pada 20, 40, 60 dan 80 pasangan telah dicambah di atas lapisan penukleusan AlN. GaN tidak terdop pada ketebalan 500 nm kemudiannya dicambah di atas struktur SLS pada suhu 1125 °C untuk mengkaji daya tahan AlN/GaN SLS untuk mengelakkan keretakan dalam sampel. Hasil dari analisa xray keluk goyang (XRC) memaparkan kelebaran penuh separa maksimum (FWHM) paling rendah dan optimum untuk 60 pasangan SLS yang mencadangkan pengurangan dislokasi dengan kenaikan bilangan pasangan SLS. Imej berjaya rentas Mikroskopi Elektron Daya Imbas (FESEM) menunjukkan struktur SLS yang baik dan mendadak manakala analisis permukaan menunjukkan permukaan lebih halus dengan kenaikan bilangan pasangan SLS. Analisis kekasaran yang dijalankan menggunakan Mikroskop Daya Atom (AFM) berhubung kait baik dengan kedua dua keputusan dari x-ray keluk goyang dan keputusan permukaan FESEM. Siasatan pada kesan melengkung juga memberikan keputusan positif di mana terdapat parameter melengkung yang optimum untuk menghasilkan GaN bebas retak di atas silikon (111). Kesimpulannya, 60 pasangan AlN/GaN lapisan menegang super kekisi boleh berjaya menampung 1 μ m GaN tidak terdop, dengan itu, menghasilkan lapisan GaN bebas retak di atas substrat silikon (111).

Kata kunci: GaN di atas silikon (111), MOCVD, bebas retak, SLS

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May this humble research achieve the blessing from Allah, the Owner of All Knowledge and a spark to more future researches.

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LIST OF SYMBOLS & ABBREVIATIONS

l	Line direction
a 0	Lattice constant in a direction
b	Burgers vector
β^2	Full width of half maximum in radian
b_{screw}^2	Burger's vector value of screw dislocation with respect to planar lattice
$b_{\scriptscriptstyle edge}^2$	Burger's vector value of edge and mixed dislocation with respect to planar lattice
C 0	Lattice constant in c direction
CMOS	Complementary metal oxide semiconductor
D _{total}	Total dislocation density inside the sample
D _{screw}	Screw dislocation density inside the sample
D_{edge}	Edge, mixed dislocation density inside the sample
F _C	Flow rate of carrier gas
FWHM	Full width at half maximum
$\mathrm{H}_{2}\mathrm{O}_{2}$	Hydrogen peroxide
P _T	Total pressure above the metal organic
Pv	Vapour pressure of the metal organic
RMS	Root mean square
TNSC	Taiyo Nippon Sanso Corporation

CHAPTER 1: INTRODUCTION

This thesis involved the studies of the buffer layer on silicon (111) substrates by using III-V nitrides material that is aluminium nitride (AlN) and gallium nitride (GaN). The epitaxial technology involved the usage of nitridation surface treatment (NST), nucleation layer and strained-layer superlattices (SLS) to compensate the lattice mismatch as well as the thermal mismatch between the III-V nitrides to realize the formation of crack-free GaN on silicon (111) substrates.

1.1 Introduction

The III-V nitrides is an interesting material to work with owing to its great potential to be used for optoelectronic applications. Most works on gallium nitride technology uses sapphire as substrate despite many limitations such as insulating property, inability of large scale uniformity and extreme hardness (Molnar et al., 1997; Liu & Edgar, 2002). Silicon (111) substrates have currently become an increasingly competent alternative substrate due to its low cost, high thermal and electrical conductivity as well as capability to be produced in large scale (Liu & Edgar, 2002; Marx et al., 1998). The most intriguing properties of silicon as a potential substrate for GaN-based devices is the practicability when integrating conventional silicon technology with GaN technology.

Nevertheless, the growth of high quality GaN epilayer on Si (111) is considered challenging due to huge in-plane thermal expansion coefficients mismatch (54 %), large lattice mismatch (16 %) and distinct crystallic structures (cubic Si against hexagonal GaN) which promotes defect in growth of GaN epilayer (Ozturk et al., 2013). Direct growth of GaN on Si (111) surface is challenging due to poor nucleation properties of GaN on Si, leading to island-like GaN structures (Uen et al., 2005). Besides that, it has been reported that at high temperature (1200 K), Si outgases and reacts with Ga causing

meltback etching (Pal & Jacob, 2004). This phenomenon promotes production of polycrystalline GaN which inhibit high quality growth of GaN.

On the other hand, cracking issue arises as major problem in the epitaxy growth of GaN/Si(111), resulting in low performance of devices due to current-scattering center for light propagations (Krost & Dadgar, 2002). Despite the problems there has been breakthroughs in growing GaN on silicon, e.g., Reiher et al. (2009) managed to fabricate InGaN/GaN LED structure grown on (110)-oriented silicon substrate. Through electrical excitation, the structure have emit light with a peak at 490 nm. However, several other works of GaN directly on Si suffers from very low quality of GaN layer and cracks that reduce the effectiveness of optoelectronic application especially for light emitting diode (LED), laser diode (LD) and high electron mobility transistor (HEMT) (Tran et al., 1999; Watanabe et al., 1993).

Outstanding improvement have been achieved in this past few years with several interesting approach. One of them is the application of Ga-free buffer layer technique to eliminate meltback etching issues. AlN were known as the most promising candidate for this approach due to smaller lattice mismatch and thermal expansion coefficient between AlN and Si as compared to GaN (Zang et al., 2004). Zamir et al. (2000) studied the correlation of AlN buffer growth temperature towards the morphological surface and preferred orientation of GaN. It is observed that the crystalline quality of GaN film was improved with increasing the AlN buffer growth temperature from 700 to 760 °C. Recently, a few groups managed to achieve good quality GaN hetero-epitaxial growth on Si(111) substrate grown by horizontal-reactor metal organic chemical vapour deposition (MOCVD). The above result were realized by addition of several layer above the nucleation layer using intermediate stacking layer of AlN/GaN (Hofstetter et al., 2006) or Al_xGa_{1-x}N/GaN (Nikishin et al., 1999), low temperature AlN interlayer (Blassing et al., 2002) and Si_xN_{1-x} interlayer (Hikosaka et al., 2014). Cracking issues were reduced

using AlN/GaN stacking layer in GaN heteroepitaxial growth which concluded the high effectiveness of the layer for strain control (Egawa et al., 2005) and for dislocation filtering (Su et al., 2015). Ubukata et al. (2007) also reported a successful crack-free GaN on 150mm diameter Si(111) with addition of 24 nm thickness/period of AlN/GaN (AlN:4nm; GaN:20nm) multilayer using horizontal flow MOCVD.

While other works focused on low growth temperature of AlN of within 650-750°C as their basis towards achieving crack-free GaN on Si (111) (Zamir et al., 2000; Bläsing et al., 2002), this work clearly highlight the ability of SR-2000 MOCVD towards achieving high quality AlN buffer layer at higher temperature growth of 1000 °C. Strained-layer superlattice (SLS) structure and nitridation surface treatment (NST) are introduced as features towards achieving high quality, crack-free GaN on Si(111) substrate.

Si(111) was chosen as the substrate for this research instead of other silicon plane due to the fact that the Si(111) plane possess two inverse three-fold symmetry that resembles the six-fold symmetry of the hexagonal GaN (0001) plane. Thus, the six main crystallographic directions of Si(111) plane can perfectly aligned to the six major crystallographic directions of the GaN in (0001) plane to form an epitaxial relationship (Liaw et al., 2000).

Towards achieving a crack free GaN layer on silicon (111) substrates by using metal organic chemical vapour deposition (MOCVD) technique, aluminium nitride (AlN) have been introduced as the potential material towards achieving that aim. The reason behind of this approach is to provide a better initial point for epitaxial growth of GaN on silicon (111) substrates. The ability of AlN to minimize cracking and compensate dislocation will be emphasized in this thesis. Besides, device quality such as LEDs performance rely mainly on the ability of buffer epitaxial to eliminate as much dislocation as possible before the LED device layer were implemented onto it. Dislocations serve as non-radiative recombination centers inside LED which reduce the internal quantum efficiency

of the photon to regenerates light. Thus, it is imperative to minimize the dislocation density within the buffer layer as it will become the key for manufacturing good quality LEDs.

1.2 Research Objectives

There are three objectives of this research towards producing a crack-free GaN layer on Si(111) substrates. The first objective of this work is to determine the homogeneity of the surface of AlN/GaN grown using MOCVD. Secondly, is to investigate the effect of varying the nitridation surface treatment (NST) time with the quality of topmost GaN layer. The third objective is mainly to investigate the effect of varying the number of period of AlN/GaN strained-layer superlattice (SLS) to the topmost GaN layer towards establishing a crack-free GaN layer on silicon (111) substrates.

Chapter 2 discusses the basics of crystal structure and the differences between silicon, GaN and AlN lattices. The theory of the crystal structures will be briefly explained. The roles of NST in the structure and the function of AlN as a potential material to filter dislocation will also be elucidated. The mechanism of MOCVD, previous works on the layer used and the modification that have been made from other researches will also be discussed in detail. Chapter 3 will described the details and the parameters of the experimental work which involved the process of cleaning the substrates, epitaxial growth and the characterizations method used to obtain the result for this thesis. Results and discussion of the overall work will be presented in Chapter 4. The structural and morphological properties of the topmost GaN layer due to the insertion of AlN and other intermediate layer will be discussed. The conclusions of this research are presented in Chapter 5.

CHAPTER 2: THEORY AND LITERATURE REVIEW

The following chapter gives a brief introduction to the physics behind this work. The necessity of introducing AIN as the nucleation layer on silicon substrate prior for the growth of a good quality GaN epilayer will be explained by understanding the crystal properties of materials as well as the difference in their crystal structures. It is also crucial to understand the behaviour of solid in high temperatures and how they response towards any temperature changes.

2.1 Introduction

2.1.1 Chemical Vapour Deposition (CVD) Techniques

The increase in demand of modern industries for increased yield and constant enhancement of material properties to be used in electronic, optoelectronic, optical and mechanical applications have prompted the development of various innovative film deposition techniques. While certain deposition techniques offers unique advantages as compared to others, each process technology has certain limitations (Wiest et al., 2006). There are three main chemical vapour deposition (CVD) techniques that is chemical vapour deposition (CVD), atomic layer deposition (ALD) and metal organic chemical vapour deposition (MOCVD).

The basic mechanism of CVD process involves the chemical reactions and/or dissociation of gaseous reactants in an activated environment (e.g. heat, plasma, light etc.) to produce high performance and high purity thin films. The conventional CVD that most commonly applied is the thermally activated CVD. This process can be categorized according to the range of pressure in which the deposition takes place. These include atmospheric pressure CVD (APCVD), low pressure CVD (LPCVD) or ultra-high vacuum (UHCVD) depending on the processing pressure. (Wu et al., 1996; Matocha et al., 2005; Kim et al., 2001). The other unique variants of CVD that have been used to deposit thin

films include metal organic chemical vapour deposition (MOCVD) [Shan et al., 1995; Fujieda et al., 1987; Manasreh, 1996; Haffouz et al., 2003; Sakai et al., 1996), plasma enhanced chemical vapour deposition (PECVD) (Humphreys et al., 1989), and atomic layer deposition (ALD) (Gates & Neumayer, 2001).

2.1.1.1 Plasma Enhanced Chemical Vapour Deposition (PECVD)

Plasma assisted or plasma enhanced CVD (PECVD) is a technique whereby electrical energy rather than the thermal energy is used to trigger the homogeneous reactions to produce chemically active ions and radicals. The ions and radicals then participate in heterogeneous reactions, leading towards the formation of thin film on the substrate (Jones & Hitchman, 2008). The main advantage of using PECVD is the ability of thin film to be grown under low deposition temperature which is often critical in the manufacture of semiconductors. Figure 2.1 shows the schematic diagram of the PECVD system (Cho & Boo, 2012).



Figure 2.1: Schematic diagram of PECVD system (Cho & Boo, 2012).

2.1.1.2 Atomic layer deposition (ALD)

Atomic layer deposition (ALD) technique has emerged as a crucial technique in deposition of thin films owing to its advantage to precisely tune the thickness of the films down to angstrom or monolayer level (Pinna et al., 2012). ALD applies unique mechanism of growth, in which monoatomic layers are deposited in sequence for a controlled-film deposition at the sub-nanometre level. Throughout the deposition process, the precursors are pulsed alternatively onto the substrate surface and subsequent chemisorption or surface reactions occurs. Due to this self-limited growth mechanism, the deposited films thickness can be precisely tailored with conformal deposition on high aspect ratio structures and excellent step coverage (Maula et al., 2011). The distinctive advantage of ALD has made it an attractive technique to be industrially applied for the deposition of very thin high-k oxides in complementary metal oxide semiconductor (CMOS) technology which serve as gate dielectrics in metal oxide semiconductor field-effect transistor (MOSFET) devices (Ye et al., 2003) and as dielectrics in the trench capacitor structures (Seidl et al., 2002). Figure 2.2 displays the schematic diagram of ALD system (Dhakal et al., 2016).



Figure 2.2: Schematic diagram of ALD system (Dhakal et al., 2016).

2.1.1.3 Metal Organic Chemical Vapour Deposition (MOCVD)

Metal organic chemical vapour deposition (MOCVD) utilizing metal organic compounds as precursors which is in contrary to conventional chemical vapour deposition technique that uses inorganic precursors, containing metal halides. MOCVD offers unique flexibility to tailor a wide range of operating conditions such as source materials, temperature and pressure to produce state of the art performance devices such as lasers, light emitting diodes (LEDs), laser diodes (LDs) and high electron mobility transistors (HEMTs) using this technique. The metalorganic source basically originate from group-III nitride films which involves high growth temperatures interacting in complex gas phase and surface reactions. The growth mechanism and the systematic surface reactions involved during growth will be explained in detailed in Chapter 2.

MOCVD is performed at much higher pressure than other CVD, allowing the group-III nitride films to be grown at significantly higher temperatures (more than 1100 °C) whereby the compound is thermodynamically stable. This favourable thermochemical condition is believed to be the main reason why MOCVD III-nitride material performs better for commercial optoelectronic device applications.

In this study, nitridation surface treatment process followed by a thin HT-AlN nucleation layer was grown on Si (111) substrate. Prior to 1 μ m growth of GaN layer, AlN/GaN multi-layer was grown beneath it, which act as the strain compensating and dislocation filtering layer. The multilayer was grown by varying the number of AlN/GaN multilayer periods of 20, 40, 60 and 80 pairs, respectively with the effort to optimize the quality of GaN epilayer grown on Si(111) substrate. This thesis reports on the crack-free GaN achieved in the sample by which the sample bowing, surface roughness and dislocation density are critically affected.

2.1.2 Crystal Structures of Material

An atomic structure which exhibit periodicity in all directions is considered as crystalline material, which consist of small building blocks called unit cells. A unit cell is the smallest periodic feature in a crystal lattice. It is defined by the unit vectors of a_1 , a_2 , a_3 . Any point of the lattice can be referred from another lattice point by using these lattice vectors. The reference lattice vectors are called the Bravais lattice of the structure, while the vector a_1 is usually interpret by the shortest period in the lattice. For cubic cells, a_2 is perpendicular to a_1 , and a_3 is perpendicular to the plane connected by a_1 and a_2 . For the lattice constant of cubic cell, $|a_1| = |a_2| = |a_3| = a$, whereby a is the lattice constant of the crystalline material (Morkoc, 2013).

The symbolization for a crystal plane is (h k l) and if the crystal planes are identically symmetry, notation {h k l} can be used. A crystal plane is determined as points in which the plane intersects the axis of the crystal lattice. The reciprocal is taken from those coordinates and they are reduced to the smallest integers. The results denoted as Miller indices of the crystal plane. It is crucial to mention that when specifying planes and directions of the hexagonal wurtzite III-nitrides as well as the various crystal surfaces, four-index Miller notation (h k i l) is usually employed where $i = \overline{h+k}$. Here, the overline is used to express a negative quantity. There are three standard notations distinctively used as follows:

(h k i l) denotes one specific plane or surface;

[h k i l] denotes one specific direction;

{h k i l} denotes equivalent planes or surfaces due to symmetry of the lattice.

The material is considered as a single crystal if it is consisted of a continuous lattice which formed by an identical unit cell. While, the material is considered to be polycrystalline, if it consists of mixed oriented grains of crystals (e.g., most metals). Other than that, the material is called amorphous if there is no long range periodicity existed.

2.1.3 Defects in Material

The properties of semiconductor materials are often tuned by two main factors which are the defect as well as the incorporation of impurities. The hetero-epitaxial layers contain large densities of native and structural defects. Among the structural defects, inversion domains, threading dislocations (TDs), pyramidical planar defects and nanopipes defects are the common defects that can cross the epitaxial layer.

It has been identified that defects can be classified as point defects, line defects, planar defects and volumetric defects. Some example of point defects are vacancies (missing atoms), interstitial atoms (additional atoms incorporated on different sites other than substitutional sites) and anti-sites (a cation sitting on a nominal anion site, or vice versa) atoms. A series of point defects create an imaginary line dislocations denoted as line defects. In an ideal polycrystalline material, the grains should be perfect crystals. However, in epitaxial growth, the grain boundaries and stacking faults (SFs) usually occur and are considered as planar defects. A line defect can also evolve into planar defect when there is array of line dislocations in a certain planar form. Whereas, volume defects are usually noted as regions and voids of amorphous material inside the grown crystal (Jasinski et al., 2003; Romano & Myers, 1997).

Dislocations are described by their line direction (l) which defines as the orientation of the dislocation in the crystal. While, Burgers vector (b) is drawn through the dislocation to illustrate the displacements inside the crystal structure. The Burgers vector originates

from the Burgers circuit, which is a loop in increments of jumps from one atom to the next that surrounds the dislocation line. When this circuit is compared to a perfect lattice, the loop opens and the additional component of the loop is the Burgers vector \boldsymbol{b} . Moreover, dislocations do not just end in a crystal; they either form a complete loop or end at a crystal surface.

The three possible types of dislocations are edge, screw and mixed-type. If l is perpendicular to b, the dislocation is an edge-type dislocation and if l is parallel to b, the dislocation is screw-type. Mixed-type dislocations are a combination of edge and screw types with b points neither perpendicular nor parallel to l. If the Burgers vector of the dislocation is a lattice vector, then the dislocation is considered a perfect dislocation. Partial dislocations happen when Burgers vectors is not equivalent to a lattice vector and are commonly referred to the decomposition of perfect dislocations also known as a stacking fault (Rockett, 2007). All dislocations discussed hereafter are perfect dislocations. Figure 2.3 illustrates screw and edge dislocations in a crystal. The arrow refers to Burgers vector with grey planes denoting the dislocation planes of each type of dislocation.



Figure 2.3: Slip systems in a hexagonal lattice with slip planes denoted in grey plane and slip directions indicated by black arrows (Jones & Batyrev, 2012).

2.2 The III-Nitride Materials

The group III-elements from the periodic table like aluminium (Al), gallium (Ga) and indium (In), when mixes with nitrogen (N) from the group V element will form a III-V compound semiconductor material system consisting of aluminium nitride (AlN), gallium nitride (GaN), indium nitride (InN), as well as their ternary and quaternary alloys. The main advantages of using III-nitride materials in semiconductor applications is mainly due to its wide coverage of bandgap energy ranges from 0.7 eV for InN to 6.1 eV for AlN as shown in Figure 2.2. Due to such wide bandgaps, group III-nitrides rapidly emerges as competence material in the development of various applications ranging from infrared to ultraviolet light emitters and high temperature with high frequency transistors.



Figure 2.4: Band gap energy vs. lattice constant for binary group III-nitride materials system (Schubert, Gessmann & Kim, 2005).

2.2.1 Crystallographic Structures

The III-nitrides present in three type of crystal structures, either cubic zincblende (ZB), hexagonal wurtzite (WZ) lattice structures and rock salt. The ZB structure is considered the metastable phase due to the degree of difficulty for it to remain in that structure for a long period of time. There are only a few works on the successful growth of the ZB structure of AlN (Gerthsen et al., 1999; Lebedev et al., 2005), GaN (As et al., 2006; Lei et al., 1991), and InN (Chandrasekhar et al., 1995; Lozano et al., 2007) by epitaxial methods. Other than that, the growth of rock salt structure is only possible under an extremely high pressure environment. While, the hexagonal wurtzite structure is reported to be very stable and the most commonly observed for III-nitrides. Therefore, this work will focus only on the WZ structure of III-nitrides. An ideal wurtzite structure comprises of two hexagonal close packed (hcp) lattices interpenetrating each other with a shift of $3c_0/8$ and exhibits the relationship of $c_0/a_0 = \sqrt{8/3} \approx 1.633$, where a_0 and c_0 are the lattice constants as shown in Figure 2.5(a). The essential building block of the wurtzite III-nitrides is a tetrahedral, with each group-III atom is bounded to four nitrogen atoms, and vice versa. However, III-nitrides did not possess the ideal wurtzite crystal structure due to imperfect tetrahedral symmetry as shown in Figure 2.5(b). The bond angle α between the [0001]-oriented bond and any other bonds is smaller than the ideal, theoretical angle of 109.5°, thus making $\alpha < \beta$ and $c_0 / a_0 < \sqrt{8/3}$. Among the III-nitrides, AlN exhibits the smallest degree of the bond angle of α with around 108.2°, suggesting that AlN crystals will experience deformation the most.



Figure 2.5: (a) Wurtzite crystalline structure and (b) A tetrahedral with the characteristics angles, α and β . In an ideal tetrahedral, $\alpha = \beta = 109.5^{\circ}$ (Thapa, 2010).

The space grouping for the WZ structure is $P6_3mc$ in the Hermann-Maugin notation (Morkoc, 2013). The group III-nitrides have partially ionic and partially covalent bonds. Due to the $1s^22s^22p^3$ electronic configuration of the N atom (the most electronegative and the smallest group-V element) and the lack of electrons occupying the outermost orbitals, the electrons in the metal nitrogen covalent bond are dominantly attracted by the Coulomb potential of the N atomic nucleus. This means that the covalent bond possesses stronger ionicity due to the large difference in the electro-negativities compared to other III-V covalent bonds, causing the III-nitrides to have high bonding energies (AlN = 11.5, GaN = 8.9, and InN = 7.7 ev/atm) (Shul & Pearton, 2011).

Figure 2.6 illustrates the wurtzite structure of hexagonal unit cell of AlN, where the Al and N sub lattice atoms, are tetrahedrally bonded to the nearest neighbours. The structure consists of stacking sequence of alternating close-packed, bi atomic (0001) planes of Al and N pairs (marked as A and B) along the c-axis. The presence of A and B bilayers results in an internal symmetry along the c-axis. This indicate that the direction of the atomic bonds is distinctive along the [0001] and [000-1] directions.

Internal polarity of the film exists due to this difference, and is described by the direction of the group-III-N bond arrangement between the two layers (along the c-axis) with respect to the normal surface of the film. If the nitrogen atoms are placed on top of the group-III atoms the film is called [0001]-polar face or Al-faced, while if the group-III atoms are on top of the N atoms the film is called N-faced or [000-1]-polar face. The polarity of the films crucially effect both the morphological properties and the piezoelectric field of the group III-nitrides. The effect of polarity has been widely studied both theoretically and experimentally in [Neugebauer, 2001; Stutzmann et al., 2001). Group III-nitrides grown on (0001) sapphire by metal organic vapour phase epitaxy (MOVPE) are typically group III-polar (Stutzmann et al., 2001). The other binaries InN, GaN, their ternaries and quaternaries have identical crystalline structure, in which group-III atoms occupy the sub-lattice shown in Al atoms position as in Figure 2.4.



Figure 2.6: Illustration of wurtzite structure of AIN (Thapa, 2010).

Technically, an unstrained AlN structure have lattice parameters of a = 3.110 Å and c = 4.982 Å, respectively (Ambacher et al., 2002). On the other hand, GaN have lattice parameters of a = 3.199 Å and c = 5.185 Å, respectively. Table 2.1 summarizes the theoretically (theo.) calculated and experimentally determination (expt.) of structural

parameters for AlN, GaN, and InN (Stutzmann et al., 2001; Ambacher et al., 2002) where a is the lattice constant in a direction, c is the lattice constant in c direction and u is the length between two nearest-neighbour anion-cation bond. Unlike GaN, the experimentally determined c/a of AlN differs significantly from the aforementioned ideal theoretical calculation parameters: c/a = 1.601 and u = 0.379 due to the strong existence of ionic bonds (Li et al., 2003). This may be the reason for the difficulties in doping of AlN. Whereas, GaN and InN have smaller iconicity than AlN (Li et al., 2003) making them easier material to be applied as n-type and p-type doped.

Table 2.1: Theoretically (theo.) calculated and experimentally determined (expt.) structural parameters for AlN, GaN and InN (Stutzmann et al., 2001; Ambacher et al., 2002).

Parameters	AIN	GaN	InN
a (theo.) (Å)	3.110	3.199	3.585
c/a (theo.)	1.633	1.633	1.633
u (theo.)	0.375	0.375	0.375
u (expt.)	0.382	0.377	0.379
a (expt.) (Å)	3.112	3.1896	3.548
c (expt.) (Å)	4.982	5.185	5.705
<i>c/a</i> (expt.) (Å)	1.60	1.626	1.608

2.2.2 Defects in III-Nitride Materials

In the case of III-nitride epilayers, the dislocations mainly originate from lattice mismatch during hetero-epitaxial growth or pre-existing dislocations from growth of the single crystal native substrate. There are three possible types of dislocations observed in III-nitrides that are: c-type with $b = \langle 0001 \rangle$, a-type with $b = 1/3 \langle 11-20 \rangle$, and (a + c)-type with $b = 1/3 \langle 11-23 \rangle$. The nomenclature of these dislocations referred directly to the directions and lattice constants in the wurtzite structure as illustrated in Figure 2.7.



Figure 2.7: Schematic view for Burgers vectors of the three types of dislocation observed in (0001) group-III nitride layers (Thapa, 2010).

These dislocations can be edge, screw, or mixed-type depending on their dislocation line. Dislocations that follow the growth direction are called threading dislocations (TDs) and have a line direction parallel to the growth direction. For example, TDs in III-nitrides grows in the c-direction have l = [0001] with c-type, a-type, and (a + c)-type dislocations being screw, edge, and mixed-type dislocations, respectively. There is another kind of dislocations that lie in a hetero-epitaxial interface and relieve misfit strain that is called misfit dislocations (MDs). For the case of III-nitride growth, MDs have l perpendicular to [0001]. MDs happened due to the difference in lattice and thermal expansion coefficient, and TDs due to the twist and tilt of crystal grains. Below specific certain epilayer thickness, known as the critical thickness, an epilayer could grow pseudomorphically on the substrate, while growth exceeding the critical thicknesses will suffer a relaxation of misfit strain via plastic flow.

During crystal growth, the unevenness of the substrate surface or the nucleation of growth islands leads to the formation of dislocations with line direction parallel to the growth direction. These dislocations penetrate the epilayer, which in turn coined as TDs and reach the growth surface except those that combined and annihilate each other. The presence of TDs significantly affects the device performances causing non-radiative

recombination (Rosner et al., 1997; Sugahara et al., 1998), carrier scattering effects (Weimann et al., 1998), and diffusion of dopants and impurities (Lebedev et al., 2005).

2.3 Substrate Comparison for Gallium Nitride (GaN) Epitaxial Growth

Nowadays, sapphire substrate has established as a conventional substrate for gallium nitride (GaN) epitaxial growth due to its considerably good properties and variable applications. However, sapphire substrate has a few limitations and disadvantages, such as its insulative properties, the incompatibility integration of device fabrication with vertical-type electrode structure, relatively low thermal conductivity to dissipate heat in high-power devices, and the limited dimension of diameter size, which make this wafer not suitable for commercial mass production of GaN.

On the other hand, hetero-epitaxy of GaN on alpha, α 6H- silicon carbide (SiC) also has been tremendously been investigated by several groups (Johnson et al., 1996; Torvik et al., 1998), with successful fabrication of electronic and optoelectronic devices, such as high electron mobility transistor (HEMT) (Kordoš et al., 2005), light emitting diode (LED) (Madhu et al., 2005), and laser diode (LD) (Domen, 1998; Edmond et al., 2004). However, due to limited availability, small diameter size restriction and the relatively far more expensive price than sapphire and silicon substrate, α 6H-SiC works have been declined in terms of publications over these recent years.

The homo-epitaxy of GaN on free-standing GaN substrate has produced a remarkable dislocation density as low as 10^6 cm⁻² (Hashimoto, 2006). Despite the superior epitaxial quality that this substrate can offer, such substrate has maximum diameter size of only 2 inches and very limited availability, which leads to its extremely expensive price. Therefore, it is only employed in high-performance devices, for which the corresponding low dislocation density is crucial such as blue-violet LD.

Although the epitaxial growth of III-nitrides on sapphire, α 6H-SiC and GaN freestanding substrate has considerably matured, there are increasing concern for the other breakthrough for GaN-based epitaxy on silicon (Si) substrate. Si have many remarkable properties, for instance, excellent availability, large diameter size of up to 12 inches and extremely low cost. The best advantage in successful growth of GaN-based devices with well-established Si-based electronic device like integrated circuits, photo-detector, and other optoelectronic devices, is basically due to the ability of allowing the fabrication of multi-function hybrid device on a single wafer.

In the comparison with conventional sapphire substrate, Si have tuneable electrical conductivity by undergoing a process known as doping and has better thermal conductivity, which greatly improves the thermal dissipation in particularly for high power with high temperature device operation. Si also are conductive in nature which allowing the fabrication of devices with vertical-type electrode structure. Table 2.2 summarizes some parameters of the substrates conventionally used with Si (111).

			GaN	AIN	Si (111)	6H-SiC	sapphire
lattice constant	a	(Å)	3.189	3.11	5.43	3.08	4.758
	с	(Å)	5.185	4.98	-	15.12	12.991
thermal		(W./cmK)	1.3	2.85	1~1.5	3.0~3.8	0.5
conductivity							
thermal	in-	$(\times 10^{6}/K)$	5.59	4.2	2.59	4.2	7.5
expansion	plane						
lattice mismatch		(%)	-	2.4	-16.9	3.5	-16
GaN/substrate							
thermal		(%)	-	33	116	33	-25
mismatch							
GaN/substrate							

Table 2.2: Comparison of substrate for GaN epitaxial growth (Nakamura et al., 2013;Takahashi et al., 2007).

Nonetheless, GaN epitaxy on Si substrate is more challenging than on sapphire or α 6H-SiC substrates. Perhaps the main drawback of epitaxy of GaN on Si was due to large thermal coefficient mismatch of 116 % between the GaN and Si which lead towards the formation of cracks during the cooling phase after growth process since the lattice constant mismatch for GaN/Si(111) of -17 % is almost similar to GaN/sapphire of 16 % as shown in Figure 2.8. Simultaneously, the mechanism of strain also happening as shown in Figure 2.9. The GaN-Si reaction during growth also forms amorphous meltback-etching layer when conventional growth technology in Figure 2.10(a) is applied. However, the above growth challenges can be overcome by controlling the epitaxial growth using buffer layer techniques to obtain high quality GaN epitaxy on Si substrate.



Figure 2.8: Mechanism of lattice mismatch in GaN grown on (a) sapphire substrate and (b) Si (111) substrate (Zhu, 2012).



Figure 2.9: Mechanism of strain happening in GaN grown on (a) sapphire substrate and (b) Si (111) substrate (Zhu, 2012).



Figure 2.10: (a) Conventional GaN epitaxial growth on Si, (b) Cracks on surface of GaN on Si, and (c) image of meltback etching (Zhu, 2012).
2.4 Achieving Crack-Free Gallium Nitride (GaN) on Silicon (111) Substrate

This research focuses on the effect of nitridation surface treatment prior to the growth of high temperature (HT) AlN nucleation layer and followed by the AlN/GaN superlattice structure (SLS) which then end with a thick GaN epilayer atop.

2.4.1 Aluminium Nitride (AlN) Nucleation Layer

It has been understandable that silicon (Si) substrates offer several challenges in growing a non-cracking homogeneous gallium nitride (GaN) epilayer on top of it. In line with this, several research groups have initiated a remarkable works in order to encounter this issue (Ableet al., 2005; Dadgar et al., 2002; Arslan et al., 2008). Epitaxial engineering knowledge have been extensively used to optimize the growth condition of epitaxial layer. The most established technique to prevent the non-cracking issue is by introducing the AlN nucleation layer on top of Si substrate.

The wurtzite structure of AIN provides the good basal plane for the subsequent growth of GaN layer on top of it. The thermal expansion coefficient of AIN also compensates the thermal expansion coefficient of GaN on Si by introducing compressive strain to the GaN layer during the cooling phase and prevent the cracking issue (Able et al., 2005). However, aluminium parasitic reaction during AIN growth deteriorates most of the works during the early stage of this approach. Moreover, the insufficient mobility of AIN to restructure on Si which causes the high tendency of AIN to produce island formation increase the dislocation site on the structure and results in bad epitaxy of GaN (Dadgar et al., 2002).

The above issue has initiated the needs to optimize the growth parameter for the AlN layer. The initial effort by using low temperature (LT) AlN in range of 650-750 °C to increase the strain compensation effect in the structure inhibit the crystal

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restructuralization of AlN and most growth suffers high dislocation when the AlN thickness is more than 10 nm (Kim et al., 2001). Although, a thin nucleation layer of AlN is good for device structure, the thickness is insufficient to prevent meltback-etching in the sample. While most works optimize the LT-AlN layer, this research will focus more on growing high temperature AlN nucleation layer to increase the surface mobility of AlN as well as to avoid island formation of AlN layer. This research will highlight the ability of HT AlN layer to coalesce and reduce the dislocation density in Chapter 4.

2.4.2 Nitridation Surface Treatment (NST) Technique

In vertical configuration LED structure, the conductivity of the topmost GaN layer is an important parameter to control. Introducing AlN into the structure will produce adversing effect depending on the thickness of the AlN nucleation layer during growth process. Thick AlN nucleation layer is insulative and prevents the steady flow of current in vertical configuration devices. Thinning the AlN nucleation layer should counter this issue but arises different problem in the epitaxy process due to insufficient thickness of AlN to prevent meltback etching into the structure. Therefore, in this work, nitridation surface treatment is introduced as preparatory layer to prevent silicon outgassing into the GaN structure. The ability to grow AlN below its critical thickness will also avoids lattice misfit in the structure due to pseudomorphic growth of layer and will reduce the dislocation inside the structure.

Recently, significant work has been reported on the growth of a single-crystalline GaN on Si substrate, where it has been realized by manipulating the growth temperature, buffer layer thickness, ammonia (NH₃) flow rate and the compound concentration. Uen et al. (2005) studied the effect of in-situ substrate nitridation temperature on the overall GaN crystalline quality where the nitridation process was conducted at 750, 950 and 1120 °C,

respectively. The applied temperature during nitridation process greatly contributes towards the surface morphology as well as photoluminescence (PL) spectra of the top GaN epilayer grown on the formed silicon nitride (SiN_x) layer. Wuu et al. (1999) showed that in order to achieve a mirror-like GaN epilayer, the pre-annealing and post-annealing of GaN growth must be optimized thoroughly. The works illustrate the dramatic reevaporation of GaN layer induced at longer annealing period with a smaller grain size. It is also reported that the NH₃ flow rate significantly improve the homogeneity of the growth GaN epilayer on Si substrate. Arslan et al. (2009) studied the effect of nitridation time on the morphological properties of GaN grown on Si(111) substrate. Selected area electron diffraction (SAED) results suggest that the crystal orientation of Si(111) was found to be transferred through the amorphous SiN_x layer into AlN and GaN layers. It is concluded that it was important to prevent thick growth of SiN_x layer which could cause a polycrystalline deposition of GaN on Si(111) substrate. Meanwhile, Ozturk et al. (2013) has published a study involving the strain analysis of GaN layer grown on nitridated Si(111) substrate using high-resolution x-ray diffractometer; in which the nitridation time highly influenced the strain generation in between each epitaxial layer.

The V/III ratio of each layer is calculated using the equation:

$$\frac{V}{III} ratio = \frac{F_{NH_3}(\mu mol / \min)}{\left(F_{TMA} + F_{TMG} + F_{TMI} + F_{SiH_4}\right)(\mu mol / \min)} \times \frac{1}{22.4 \times 10^6}$$
(2.1)

Since nitridation surface treatment only involve the flow of ammonia (NH₃) without any flow of group III precursor, the V/III ratio is not considered for that layer. The V/III ratio is one of the main parameter which determines the growth direction and preferred surface orientation of each layer. Furthermore, the crystal quality is closely related with the change in V/III ratio of each layer. Yang et al. (2000) highlighted the influence of V/III ratio in the low temperature aluminium nitride (LT-AlN) interlayer towards the crystal quality of the topmost GaN layer. The author concluded that V/III ratios of the LT-AIN interlayer could greatly affect the crystal quality of GaN, instead of the strain status. Such dependence could be explained in terms of the different LT-AIN surface morphologies originating from the tunable V/III ratios and the consequential distinct GaN growth rates in vertical and lateral direction. The LT-AIN grown with optimizing V/III ratio can efficiently avoid the propagation of the thread dislocations in the structure of GaN epitaxial.

Dadgar et al. (2003) and Krost et al. (2003) also found that both the thickness and the growth temperature of LT-AlN layer could strongly influence the strain relaxation status and the overall quality of the GaN layer grown on LT-AlN interlayer respectively.

2.4.3 AIN/GaN Strained-layer Superlattice (SLS)

Multilayer and/or strained-layer superlattice (SLS) epitaxial technique is significant to control crack generation in III-nitride growth. During cooling phase of MOCVD growth, the reactor temperature ramp-down to room temperature and generates bowing effect into the sample due to different lattice coefficient of materials of each layer. It generates concave wafer curvature and cracks on the epitaxial layer due this difference, which leads to difficulty in producing thick GaN epitaxial layer. SLS is also effective to reduce misfit dislocations resulted from lattice mismatch of GaN-based epitaxial layer and the underlying Si substrate. Threading dislocation (TDs) can be modulated to prevent them from penetrating to the surface using SLS due to the abruptness in lattice change between AlN and GaN below their critical thickness.

When a stack of two types material with different lattice constant is grown coherently, lattice strain is built upon the interface of the two different materials producing a strong strain effect on the overall SLS layer when accumulated together. Therefore, TDs which reach the SLS interface are bent by the strain, and reaction between inclined TDs will create dislocation close-loop, preventing the TDs from penetrating vertically into the device layer. The SLS structure creates multiple built-up interface strain for TDs inclination to happen, thus, preventing dislocation to reach the topmost GaN layer. If the lattice strain is weak, it is not possible to bend the threading dislocations causing it to penetrate through the structure (Gian et al., 1996). Meanwhile, SLS with too large lattice strain will generate production of new misfit dislocation. Thus, the SLS thickness, abruptness and repeatability of each layer should be precisely controlled so that the SLS function effectively as dislocation filtering layer.

In vertical flow MOCVD, abrupt and uniform SLS is almost impossible to grow due to the deposition mechanism and the flow of precursor which have high tendency to produce air turbulence during growth of SLS (Meng et al., 2013). This research takes the advantage of using horizontal flow MOCVD which able to produce a uniform, steady flow of precursor throughout the deposition process to produce a very uniform and abrupt results with precise repeatable layer in which the are shown in Chapter 4.

2.5 Metal Organic Chemical Vapour Deposition (MOCVD)

The first MOCVD growth in the world was done by Manasevit & Simpson (1971), two chemists working at Rockwell corporation who coined the term "metal-organic" (MO) emphasizing the metal component and further published literatures describing the MOCVD of III-V semiconductors including GaN and AlN, demonstrating the flexibility of this process. Since then, MOCVD have been one of the dominant industrial processes for the fabrication of semiconductor and optoelectronic devices as it offers the advantage of conformal step coverage and deposition over a large scale. The basic working mechanism of MOCVD is to carry precursor materials into a deposition chamber where they are uniformly distributed over the surface of the substrate and decompose via pyrolysis to produce a uniform epitaxial layer of material. The most commonly used source of nitrogen for the III-nitrides growth is anhydrous ammonia, a liquid which has a sufficiently high equilibrium vapour pressure at room temperature which then been delivered directly to the deposition chamber as a gas.

The most commonly used MO sources are trimethylaluminium (TMA), trimethylgallium (TMG) and trimetyhilindium (TMI). At room temperature, TMA and TMG are liquids while TMI is solid, in order to abstain them from being delivered directly into the chamber. The three MO were packed in sealed metal containers, known as bubblers, due to their pyrophoric nature. In order to transport the MO materials to the reactor, a carrier gas mainly hydrogen and/or nitrogen is flowed into the bubblers where it goes through a plunge tube submerged in the MO. The carrier gas becomes saturated with the vapour phase MO that is present above the liquid level after "bubbling" process. The carrier gas then delivers this vaporized MO into the reactor.

The important factor that should be taken into account is the amount of MO that is being delivered into the reactor. The amount of MO delivered into the reactor depends on the equilibrium vapour pressure and typically calculated in micromoles. The flow rate of MO material out of the bubbler in moles/minute can be calculated as:

$$M_{OM}(mol/\min) = \frac{F_C(sccm)}{22,400(cm^3/mol)} \times \frac{P_V}{P_T - P_V}$$
(2.1)

where F_C indicates the flow rate of the carrier gas, P_T is the total pressure above the MO, and P_V is the vapour pressure of the MO. The vapour pressure of the MO can be modelled for a specific material at absolute temperature *T* using the parameters *a* and *b* by the equation

$$\log(P_v) = a - b/T \tag{2.2}$$

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By referring to Equation 2.2, the exponential temperature dependence of P_{ν} needs the bubblers to be dip in chilled water baths to avoid fluctuation in temperature which can disturb the constant uniform delivery of MO. The ammonia can be considered as an ideal gas with the molar flow rate calculated using the equation:

$$M_{NH_3}(mol/\min) = \frac{F_{NH_3}(sccm)}{22,400(cm_3/mol)}$$
(2.3)

The ratio M_{NH_3}/M_{OM} calculated from Equations 2.3 and 2.1 is termed as the V/III ratio and is a very useful parameter to describe the growth processes to determine the properties of the deposited material. Hydrogen and nitrogen is the carrier gas that were used in SR-2000 MOCVD system. It is noted that hydrogen gas is more suitable for thicker layer of deposition while nitrogen is efficiently useful for growing thin layer of material. Nitrogen is also preferred to be used for processes involving indium since hydrogen has an adverse impact on indium corporation.

The hydrogen pellet and ammonia are stored in high pressure gas cylinders that are reduced by a systematic pressure regulators flow system located in the gas yard before they are connected to the system. On the other hand, nitrogen was kept in the form of liquid in a big nitrogen tank which are pressurized to become gas to be used by the system. From there, the gases and the MOs that flow through the system is electronically controlled by using a vast system of mass flow controllers (MFCs), pneumatic valves and pressure controllers. The MFC consists of a main gas flow cavity through which the flow is being regulated using an electronically controlled valve. A small portion of the flowing gas is carried into a capillary tube from the flow cavity with two thermalled temperature sensors. The flow rate can be determined based on the temperature different of the sensors in the capillary tube following this equation

$$q = FC_p \Delta T \tag{2.4}$$

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where q is the heat lost, F is the flow rate, C_p is the heat capacity, and ΔT is the change in temperature. Obtaining this information, the control valve adjust electronically to match the flow to the given set point. The dependency of the flow rate calculation towards specific heat capacity of certain gas requires the MFC to be calibrated for a specific gas.

Due to the number of crucial elements involved, an automated system is essential in handling the gas system. A computer is usually connected to the mainboard of the MOCVD system, with a programmable logic controller (PLC) acting as an intermediate interface between the computer and gas handling components such as valves and MFCs. The PLC applies a set of safety interlocks, which are constantly checked before any commands is executed from the computer. It provides safety features which guards the user from mistakes or malfunctions which cause certain undesirable routing problems such as toxic gas leaking into the environment.

The MOCVD growth chamber is where the formation of thin films take place. The growth chamber design is very important for the MOCVD process to a degree that by having the same identical design of chamber and flow channel then only a growth can be identical in terms of result and quality. There are basically two common types of MOCVD that depends on the way the gas will flows into the MOCVD chamber, the vertical and horizontal MOCVD. In the vertical configuration, the gases are introduced from the top inlet, and perpendicularly flow downward onto the substrate placed on the susceptor. While in the horizontal reactor, the gases are flowed horizontally from the three-layered gas injection nozzle inlet and stream tangentially to the growth site. The top nozzle carries hydrogen and nitrogen gas known as gas carry to counter balance the pressure from the other two lower inlets.

The middle inlet transport the MO sources to the growth sides by means of carrier gases such as hydrogen and nitrogen gas. Whereas, the bottom inlet carries ammonia to be used as nitride element during the deposition. Figure 2.11 illustrates the incoming gas process entering the horizontal flow reactor through the three-layered gas injection nozzle inlet. The main advantage of using horizontal MOCVD as compared to vertical MOCVD is due to the capability of producing a very uniform and homogenous growth layer on the substrate and thus increasing the yield of deposition per unit area per wafer.



Figure 2.11: Process gases enter the horizontal flow reactor through the three-layered gas injection nozzle inlet ("Side inlet design illustration", 2017).

The fundamental necessity for the efficient control of MOCVD deposition process lies in the ability of the MOCVD to retain the laminar flow during growth. It is a well-known that, the turbulence gas effect that usually occurred inside the chamber can be avoided under laminar flow condition. This property lead towards a uniform layer of thin film to be deposited. The other factor that contributes to the uniformity of the grown thin film layer is the rotating disk that is connected to the stage inside the reactor where the susceptor is placed upon. It consists of a rotating disk as the susceptor which holds the wafer and rotate at a desirable speed (normally set to 10 rpm) against a continuous stream of gases flowing toward it at a normal angle. All the way during growth process, the disk will rotate at a fixed rotation which providing a stable, homogenous and uniform layer of thin film throughout the entire substrate surface. Figure 2.12 shows the schematic illustration of MOCVD process that ensues on the substrate during growth.



Figure 2.12: Schematic illustration of MOCVD growth mechanism (Nagendra, 2009).

In general, the MOCVD process involves the following crucial steps:

- 1. Formation of active gaseous reactant species.
- 2. Transport of the reactant species into the reaction chamber.
 - a. The precursor or MO in the form of vaporized reactants is transport into the chamber by carrier gas (reactive gases such as hydrogen or inert gas that is nitrogen).
 - b. The delivery of reactants directly depends on the carrier gas flow rate, pressure of the MO bottle and the source/bubbler temperature as indicated in equations 2.1 and 2.2.
 - c. High purity (i.e. 99.9999 %) gaseous reactants or carrier gas is being used with flow rate being precisely controlled using mass flow controllers (MFC).
- 3. Gaseous reactants undergo gas phase reactions creating intermediate species.
 - a. The precursors react with NH₃ at a high temperature leading to homogeneous gas phase reaction, where intermediate species can be formed which further undergo subsequent decomposition and/or chemical reaction, producing powders and volatile by-products in the gas phase.

- b. Below the dissociation temperature of buffered phase, diffusion of intermediate species across the boundary layer occur. The diffusion rate depends on the parameter of the deposition such as temperature, pressure, concentration of the precursor and the design of the reactor.
- 4. Absorption of gaseous reactants onto the heated substrate surface and the heterogeneous reaction occur. The process result in deposit and by-product species.
- 5. The diffusion of the deposits along the heated substrate surface creating the crystallization centre and the growth of the film is initiated.
- Unreacted gaseous precursors and by-products will be evacuated away from the deposition chamber to exhaust.

CHAPTER 3: RESEARCH METHODOLOGY

This chapter describes an overview of the process for nitridation surface treatment (NST), deposition of aluminium nitride (AlN) nucleation layer and AlN/GaN strained-layer superlattice (SLS) using the reactor described in the previous chapter. The detailed steps and flow of the experiment are described concisely.

3.1 Substrate Cleaning

The silicon (111) wafer undergoes the substrate cleaning process before being deposited in metal organic chemical vapour deposition (MOCVD) reactor. There are mainly three subsequent steps in the cleaning process for silicon (111) wafer that is the organic cleaning, the Radio Corporation of America standard cleaning (RCASC) method and lastly the hydrofluoric acid (HF) dip cleaning (Bachman, 1999).

3.1.1 Organic Cleaning/Solvent Cleaning Method

The silicon (111) wafer were immersed in a contained beaker filled with acetone inside the water bath at temperature of 50°C for 10 minutes. Consequently, the substrates were rinsed in deionized (DI) water for 5 times. The acetone dip steps were repeated thoroughly for one more time. After the second acetone dip was carried out, the silicon wafer were submerged in propanol to remove the acetone residue on the surface of the substrates. The contained beaker of propanol with the wafer were put in the water bath for 10 minutes before being rinsed with DI water for another 5 times. After that, the wafer were dried using nitrogen blowing on the surface of the silicon wafer.

3.1.2 Radio Corporation of America Standard Cleaning (RCASC) Method

This cleaning method was developed by Werner Kern and functioned to remove organic residues and particles on the silicon wafer surface (Bachman, 1999). The treatment is by introducing a thin layer of silicon dioxide (SiO₂) layer on the silicon surface with a certain degree of metallic contamination that shall be removed in the subsequent cleaning steps. The RCASC involved the heating of 65 ml of ammonia solution (NH₄OH) to 70 +/- 5 °C using hot plate. The next step involved the mixing of 65 ml of hydrogen peroxide (H₂O₂) into the solution. The magnetic stirrer were used to stir the solution well. The indicator for a good mixture of RCASC is the vigorously bubbling effect that can be observed one minute after the stirring process takes place. The silicon (111) wafer were then immersed in the RCASC solution for 10 minutes before being rinsed with distilled water for 5 times. The silicon wafer were then dried using nitrogen blowing. The RCASC solution can be reused within 24 hours at room temperature and 30 minutes at 70 °C.

3.1.3 Hydrofluoric (HF) Acid Dipping Method

Hydrofluoric acid (HF) is mainly used to remove the native silicon dioxide layer which is formerly produced during the RCASC cleaning method. Due to the reactive nature of HF which easily corrodes glass container, only polypropylene container and syringe were used during the overall process. 480 ml of DI water and 20 ml of HF were stirred slowly for 1 minute to produce the solution of HF before the silicon (111) wafer were dipped for 5 minutes. The silicon (111) wafer will then undergoes simple wetting test as an indicator for checking the effectiveness of HF dip process. Little deionized (DI) water were poured on the surface of the wafer to check the hydrophobicity of silicon wafer. If the water rolls of and beads up, the surface is hydrophobic. Since pure silicon is hydrophobic and oxide is hydrophilic in nature, a non-wetting surface suggests an oxide-clean surface. The silicon wafer were then dried with nitrogen blowing before being put into the metal organic chemical vapour deposition (MOCVD) reactor for deposition process. The HF solution can be reused for repeated cleaning process since it does not lose its effectiveness with time. The overall cleaning process takes around 1 hour and 30 minutes and Figure 3.1 shows the schematic flow of silicon (111) cleaning process.



Figure 3.1: Schematic flow of silicon (111) cleaning process.

3.2 Metal Organic Chemical Vapour Deposition

Metal organic chemical vapour deposition (MOCVD) that were used throughout this experiment was from Taiyo Nippon Sanso Corporation (TNSC) model SR-2000 which have the capability of growing up to 4 inch wafer inside the reactor. For the purpose of preliminary serial of experiment and the suitability of budget, 2-inch silicon (111) wafers were chosen as the substrate throughout this research. The reactor is a laminar flow MOCVD design which inhibit turbulences in the gas flow resulting in precise control of film thickness and material composition. The metal organic (MO) precursor compounds employed in this experiment are trimethylgallium (TMGa), trimethylaluminum (TMAI) and ammonia gaseous (NH₃) which provides the reactant source materials for Gallium (Ga), Aluminum (Al) and Nitrogen (N) respectively. Hydrogen (H₂) and nitrogen (N₂) gas was supplied as the gas carrier to accommodate the transport of MO into the reactor along the epitaxial growth.

3.2.1 Hydrogen Thermal Cleaning

The process was initiated immediately after the cleaning process by treating the silicon surface by using in-situ hydrogen cleaning method inside the MOCVD reactor. The transferring process from the nitrogen blowing site to the metal organic chemical vapour deposition (MOCVD) reactor usually produce a thin layer of native oxide layer due to the high reactivity of oxygen with silicon surface. Thus, in order to remove the native oxide layer on the surface, hydrogen cleaning was carried out on the surface of the wafer by heating the substrate to a deposition temperature of 1125 °C while flowing hydrogen into the chamber for 10 minutes.

3.2.2 Controlled Preliminary Sample

In order to prepare the Si substrate for the subsequent growth process, the nitridation surface treatment (NST) was carried out by supplying an ammonia (NH₃) flow of 5 slm at 1000 °C for 400s. After the NST process, a 20 nm aluminium nitride (AlN) nucleation layer is grown at the same temperature followed by growing a 20 pairs of aluminium nitride/gallium nitride (AlN/GaN) multi-layer with thickness of 11 nm and 13 nm, respectively. Finally, a 500 nm thick of undoped gallium nitride (ud-GaN) epilayer was grown atop. This deposition is the first preliminary experiment to determine the initial condition of the growth. Figure 3.2 shows the growth structure of the preliminary sample.



Figure 3.2: Growth structure of preliminary sample.

3.2.3 Aluminium Nitride (AIN) Nucleation Layer Homogeneity Test

After obtaining the result for the preliminary experiment, with an effort to study the homogeneity of high temperature aluminium nitride (HT-AIN) layer, the thickness of HT-AIN were varied to three different thickness of 50, 100 and 200 nm, respectively. The reason for carrying out the homogeneity test is to analyse the capability of SR-2000 to produce a stable thin film of AIN nucleation layer as a preparation for the subsequent growth of AIN/GaN strained-layer superlattice (SLS) on top of it. The second reason is to determine the effect of surface uniformity of HT-AIN at different thickness towards the topmost GaN layer. The resulting effect was then observed on the top gallium nitride (GaN) layer while maintaining the parameters of the other layer. Figure 3.3 shows the schematic growth structure and the varied parameter of the AIN nucleation layer.



Figure 3.3: Schematic growth structure and the varied thickness parameter of the AlN nucleation layer.

3.2.4 Influence of Nitridation Surface Treatment (NST) Growth Time Against the Quality of the Gallium Nitride (GaN) Layer

Consecutively, in order to study the influence of nitridation time towards the quality of the growth top gallium nitride (GaN) layer, the epitaxial growth process was repeated while varying the nitridation layer growth time to 40, 220 and 400 seconds. The parameters for the other layers are kept constant while the aluminium nitride layer thickness was fixed to 20 nm. The reason of using 20 nm for the aluminium nitride (AIN) nucleation layer originates from the idea that in term of device performance, thin AIN nucleation layer performs better when compared to thicker nucleation layer (Lahreche et al., 2000). This is due to aluminium properties which have a wide band gap of 6.2 eV. The wide band gap acts as a barrier for the conduction of electron from the valence to the conduction band. A thick layer of barrier increased the threshold voltage of device and thus, reduce the current conduction in optoelectronic devices such as light emitting diode and laser diode. However when the thickness of the AIN is thin enough (approximately 20 - 30 nm) the electron can easily tunnels from valence to conduction bands and reduce the threshold voltage of the devices.

On the other hand, if the AlN nucleation layer thickness is too thin (approximately ~5 nm), the hydrogen might etch the AlN nucleation layer back creating a rough amorphous layer of AlN. Meltback etching dominates the growth, which induces the polycrystalline growth of gallium silicide in the sample. On top of the AlN nucleation layer, 60 pairs of AlN/GaN SLS was deposited to prevent the threading dislocation density from propagating up the substrate and contributes to higher dislocation density in the sample. The reason for choosing 60 pairs of SLS is to ensure the topmost GaN is crack-free. The effect of the nitridation surface treatment (NST) growth time was evaluated by analyzing the topmost GaN layer. Figure 3.4 shows the schematic growth structure and the varied parameter of the nitridation surface layer.



Figure 3.4: Schematic growth structure and varied nitridation time.

3.2.5 Effect of Varying the Aluminium Nitride/Gallium Nitride (AlN/GaN) Strained-layer Superlattice (SLS)

After analysing the characterization result of the earlier series involving both the nitridation layer and the aluminium nitride (AlN) nucleation layer, a new series of experiment was conducted to study the effect of varying the number of period of aluminium nitride/gallium nitride (AlN/GaN) strained-layer superlattice (SLS) pairs on the quality of the topmost GaN layer. The number of period of AlN/GaN SLS was varied to 4 different pair numbers of 20, 40, 60 and 80 pairs, respectively. The nitridation surface treatment was done for about 400 seconds and the thickness of the AlN nucleation layer was fixed to 20 nm. The effect of varying the pair numbers against the whole structure performance was determined by evaluating the topmost GaN layer of the sample. Figure 3.5 shows the schematic growth structure and the varied parameter of the AlN/GaN SLS.



Figure 3.5: Schematic growth structure and varied number of AlN/GaN SLS pairs.

All the sample sets were compared with the controlled preliminary sample to investigate the effect of variation of parameter of each layer. Figure 3.6 shows the overall experimental flow for this research towards achieving crack-free growth of GaN on Si (111) substrate.



Figure 3.6: Schematic diagram of experimental method.

3.3 Sample Characterizations

The properties of the as-deposited samples were investigated using various characterization methods. Total of 10 samples were examined using various characterization methods to determine its properties. The surface morphological properties of the topmost GaN epilayer grown on Si (111) substrate were analyzed by Park System (XE-100 Model) atomic force microscopy (AFM) and Hitachi (SU8000 Model) field effect scanning electron microscopy (FESEM). Next, surface profilometer was used to evaluate the degree of wafer bending or wafer bowing in the sample. The wafer bowing is measured using surface profilometer across the whole wafer and was determined to be the height difference between the center and the edge of the Si substrate. Subsequently, the full width at half-maximum (FHWM) of both symmetric and asymmetric ω-rocking curves were measured by x-ray rocking curve (XRC) measurement using PANalytical XRD to determine the crystallinity of the topmost GaN layer. Quantitatively, the screw, edge and the total dislocation density of all the samples were calculated.

CHAPTER 4: RESULT AND DISCUSSION

4.1 Introduction

This chapter will show the results of the deposition throughout this research. A preliminary sample was first deposited and characterized to provide the initial growth results for gallium nitride (GaN) grown on silicon (Si) (111). Next, 3 sets of variation in growth parameter consisting of three different layers in the structure were deposited and the results were compared and analysed with respect to the first controlled growth condition. The effect of changing the parameter is described in detail.

Two types of characterization were done on the sample involving the morphological and the structural properties of the topmost GaN layer grown under different growth parameter. The surface morphology of the topmost GaN layer were analysed using atomic force microscopy (AFM) where the average surface roughness and peak to valley value are determined. In order to confirm the morphological structure of the sample, surface scanning was carried out using field effect scanning electron microscopy (FESEM) measurement.

Hetero-epitaxial deposition which involves the stacking of two distinct materials with different thermal expansion coefficient is expected will induces the bending effect on the sample. Thus, as a step to determine the degree of wafer bending inside the sample, profilometric scan was done across the surface of the 2 inch wafers. Next, x-ray rocking curve (XRC) measurement was carried out using high resolution x-ray diffractometry (XRD) analysis at both symmetric and asymmetric plane of GaN to determine the type as well as the value of dislocation density that is generated at the topmost GaN layer. The function and the importance of each layer in altering the dislocation density for each growth will properly be discussed in detailed.

Chapter 4.2 will highlight the results and discussion of the preliminary growth condition. While Chapter 4.3 will discuss more on the homogeneity test of aluminium nitride (AIN) which includes the comparison of results with the preliminary sample. The importance of producing a thin uniform layer of AIN is also discussed from device perspective. Chapter 4.4 will analyse the effect of optimizing the nitridation time towards the quality of the topmost GaN layer. The importance of nitridation surface treatment as second in-situ growth preparation steps is highlighted accordingly. Chapter 4.5 will show the result of varying the number of AIN/GaN strained-layer superlattice towards the overall quality of the topmost GaN layer. The function of AIN/GaN SLS as dislocation filtering will be discussed in detail. Lastly, Chapter 4.6 will highlight the main achievement of this research in producing crack-free GaN epitaxy up to 1 micron on Si (111) substrates. The relationships and the importance of each layer in producing a good epitaxial deposition will be discussed in this chapter.

4.2 Controlled Preliminary Growth of GaN on Si (111) Substrates

The first preliminary growth parameter of GaN on Si (111) substrates was determined based on several initial commissioning recipe during the installation period of metal organic chemical vapour deposition (MOCVD) equipment at University of Malaya back on February 2014. The growth parameter of each layer is summarized in Table 4.1.

Epitaxial Layers	Growth	Growth temperature	V/III	Growth
	pressure (kPa)	(°C)	ratio	Time (s)
GaN	13.3	1125	4800	670
(topmost layer)	15.5	1123	1000	070
AlN/GaN SLS	13.3	1125	2800	12 (nor noir)
(20 pairs)				45 (per pair)
AlN nucleation	13.3	1000	2800	69
layer (NL) bottom)				

 Table 4.1: Growth parameters of each layer of initial preliminary sample.

From the above growth parameter, the nitridation and the aluminium nitride (AlN) nucleation layer (NL) were grown at a homogeneous condition of 13.3 kPa and 1000 °C growth temperature. This two layers were considered the first buffer and plays a vital role in producing a good quality of GaN layer. The surrounding pressure was remaining the same throughout the whole growth process to inhibit turbulence effect which will deteriorates the uniformity of epitaxial layer during nucleation and growth process.

4.2.1 Morphological Properties

The morphological structure of the preliminary sample was first determined by simple observation using naked eyes. The sample appears cloudy and shows crack propagating throughout the sample with some white spot on the sample. The sample was further analysed by surface scanning using field effect scanning electron microscopy (FESEM). Figure 4.1 shows the FESEM image of the cracks generated on the topmost GaN layer for the preliminary sample.



Figure 4.1: FESEM image of topmost GaN layer of preliminary sample.

The cracks were generated across the sample with most of them propagating near/from the white spot region as can be seen in the image. The white spot is concentrated mainly at the edge of the wafer and contributes toward the generation of cracks. Such condition has often been observed in many publications referring to the phenomenon known as the melt-back etching of silicon. Ishikawa et al. (1998) observed the same phenomenon at higher degree of melt-back etching. According to the experimental results, the surface morphology of GaN films will significantly degraded as growth proceed once the meltback etching happens. Favorably, addition of intermediate superlattice buffer layer can eradicate the melt-back etching of GaN/Si. The multi pairs of superlattice interlayer can effectively counter the formation of large voids and profound cracks which are the main pathway for melt-back etching trajectories.

When compared to the parameter of this preliminary growth, the AlN/GaN SLS multi pairs have been inserted into the overall structure. Despite that, interestingly it is found out that by insertion of 20 pairs of AlN/GaN SLS layers, the melt-back etching cannot be prevented during growth process. It is believed that the gallium silicide formation happens mainly due to the outgassing of silicon during high growth temperature of AlN up to 1000°C. During this stage, the silicon diffuses out from the thin AlN layer and reacts with gallium precursor during the latter growth of GaN layer. The evaporated silicon will become residue on the wall of the flow channel and melt-back during the growth of GaN layer at 1125 °C. Due to high reactivity of gallium metal with silicon, they form polycrystalline gallium silicide that deteriorates the surface of the GaN layer. The turbulence effect of precursor and gas flow during growth process inhibits the formation of single crystalline GaN due to the formation of polycrystalline gallium silicide on the layer.

Due to the above reason, the AlN nucleation layer (NL) thickness have been increased in the next phase of experiment due to the fact that the AlN layer is too thin to prevent the silicon from outgassing into the GaN layer. During this stage of research, the idea to increase the AlN/GaN SLS number of pairs to prevent threading dislocation was not yet taken into consideration. In order to confirmed the hypothesis regarding the generation of melt-back etching, atomic force microscopy (AFM) technique have been used to investigate the roughness and the peak to valley of the topmost GaN layer. Figure 4.2 shows the 5 micron \times 5 micron result of 3 dimensional AFM view of the preliminary sample.



Figure 4.2: 5 μ m × 5 μ m AFM image of preliminary sample.

The topmost GaN layer exhibits root mean square (RMS) surface roughness of 1.9 nm with peak to valley value of 5.083 nm. When compared to Zhe et al. (2007) results, the sample with melt-back etching layer also exhibits the same range of RMS surface roughness as in the preliminary sample. The rough surface of GaN suggest the formation of polycrystalline GaSi during the formation of GaN layer. The bowing effect on this preliminary sample was recorded at 67 μ m. Krost et al. (2005) investigates the effect of bowing towards the GaN surface on Si and concluded that the wafer bowing caused by tensile and compressive stresses during the epitaxial growth leads to a temperature fluctuation at different positions on the wafer. Higher bowing effect deteriorates the uniformity of the topmost GaN layer and induces the formation of crack.

4.2.2 Structural Properties

The structural properties of the sample were determined from the full width half maximum (FWHM) of x-ray rocking curve (XRC) measurement. The dislocation density was calculated using the equation below (Zheng et al., 2003):

$$D_{screw,edge} = \frac{\beta_{(002),(102)}^2}{9b_{screw,edge}^2}$$
(4.2)

where the β^2 is the full width of half maximum in radian, b_{screw}^2 is the Burger's vector value of screw dislocation with respect to planar lattice b_{edge}^2 is the Burger's vector value of edge and mixed dislocation with respect to planar lattice. (002) and (102) plane are selected to be analysed as this peak associated directly with the dislocation density inside the sample (Krost et al., 2005). It is crucial to denote that one mixed dislocation consists of the displacement of one screw dislocation plus one edge dislocation. Therefore, the mixed dislocation is mistakenly being overestimated (Krost et al., 2005). In this research, the b_{screw}^2 value used is 5.185×10^{-8} cm⁻² and the b_{edge}^2 value used is 3.189×10^{-8} cm⁻² (Zheng et al., 2003). The screw together with mixed and edge dislocation density are determined from the FWHM of XRC scanning along the symmetric and asymmetric plane of GaN surface. Figure 4.3 shows the (002) and (102) scan of topmost GaN layer using XRC technique.



Figure 4.3: XRC scan of (002) (left) and (102) (right) plane of the topmost GaN layer of the preliminary sample.

The FWHM for (002) and (102) XRC scan are 2502 and 4698 arc sec, respectively. The value is comparatively high as suggests by the high cracking density and big cracking gaps on the sample as viewed by FESEM image. The screw dislocation is calculated to be 6.08×10^9 cm⁻² and 5.67×10^{10} cm⁻² for the mixed and edge dislocation. The value provides the basic initial result to be used as comparison when optimizing the parameter of each layer in the next phase of experiment. Such dislocation appear due to different lattice mismatch in between AIN and GaN during growth (Bai et al., 2006). When compared to works reported by Sakai et al. (1998) and Bourret et al. (2001), this preliminary sample already experience a tremendous reduction in total dislocation density by a factor of 2 from the achievement of previous works for dislocation in range of $10^{11} \sim 10^{12}$. The total dislocation density is then calculated using equation:

$$D_{total} = D_{screw} + D_{edge} \tag{4.3}$$

whereby, D_{total} is the total dislocation density inside the sample, while D_{screw} and D_{edge} is the screw and edge, mixed dislocation density inside the sample. Table 4.2 summarizes the structural and morphological properties of the preliminary sample as reference to be compared after the change of parameter of other layer in the next phase of experiment. In terms of device performance, FWHM analysis provides initial quantitative analysis of dislocations inside the sample. Higher dislocation density contributes towards lower device performance as dislocations act as non-radiative recombination site in LED device.

Properties	Value / Observation	
Naked – eye Observation	Cloudy sample. Crack generated across the surface of GaN.	
FESEM surface imaging	Meltback etching observed. Generation of large micro-crack and smaller micro-crack especially near the metlback etching site.	
RMS roughness $(5 \times 5 \ \mu m^2)$ (nm)	1.9	
Peak to valley (nm)	5.083	
Bowing value (µm)	67	
FWHM of (002) XRC scan (arc sec)	2502	
FWHM of (102) XRC scan (arc sec)	4698	
Edge dislocation density (cm ⁻²)	6.08×10^{9}	
Screw dislocation density (cm ⁻²)	5.67×10^{10}	
Total dislocation density (cm ⁻²)	6.28×10^{10}	

Table 4.2: Structural and morphological properties of preliminary sample.

4.3 Homogeneity Test for AlN Nucleation Layer

This topic will discuss the importance and the needs to investigate the surface homogeneity of AlN between the silicon and the AlN/GaN SLS surface. The results of varying the AlN thickness on the topmost GaN layer is further discussed and compared with the preliminary sample.

4.3.1 Importance of Homogeneity Test

The inability to grow smooth surface of thick low temperature AIN (LT-AIN) between silicon and gallium nitride layer have limits the extension of research towards developing a thick AIN layer to be used in ultraviolet (UV) applications especially in UV laser diode (LD) and UV light emitting diode (LED). Previous researches on LT-AIN also produces bad structural quality of AIN due to the low surface mobility of aluminium during recrystallization or restructuralization process. While most researches on LT-AIN tunes the other growth parameter such as V-III ratio and pressure to provide coalesce surface of AIN, this thesis highlighted the usage of high temperature of AIN as nucleation layer towards achieving a homogeneous surface of AIN.

4.3.2 AIN Nucleation Layer Homogeneity Test

The highlighted parameter to be varied is the thickness of AlN where this lead towards the investigation of the effect on the topmost GaN layer. The AlN thickness was varied to 3 different thickness of 50, 100 and 200 nm while all parameters for the other layers were kept constant. The sample were analysed on the topmost GaN layer in term of structural and morphological properties. After the samples were taken out from the MOCVD reactor, naked-eye observation shows a positive trend of reflectivity of the topmost GaN surface as the thickness of AlN is increased. The sample is cloudy when 50 nm thickness of AlN nucleation layer is grown. As the AlN NL thickness is increased to 100 nm, the surface become less cloudy. An increase of AlN NL thickness to 200 nm results in a specular and mirror-like surface of topmost GaN layer.

4.3.2.1 Morphological Properties

Cross-section scanning using field effect scanning electron microscopy (FESEM) technique was conducted to further confirm the homogeneity of grown AlN nucleation layer on Si (111) substrate. Figure 4.4 shows the cross section images of the samples with varied AlN nucleation layer thickness. From Figure 4.4(a), the growth rate of each layer is calculated and the thickness of each layer is carefully tuned to acquire a more accurate thickness as shown in Figure 4.4(c). At 100 nm thickness, as in Figure 4.4(b) the AlN layer exhibits 3 dimensional growths with high peak to valley value as estimated from the cross section image of FESEM. The 3 dimensional growth promotes the generation of cracks and wafer bowing on the sample which produces cloudier surface when seen using naked eyes. Zang et al. (2004) highlighted the issue of 3 dimensional growths of AlN on Si. It is stated that 3-dimensional AlN nuclei were formed on silicon substrate during initial growth stage (varying from several seconds to several minutes). These nuclei grew with very dominant lateral growth rates compared to vertical growth rates, due to the wetting conditions of AlN after TMA pre-treatments. This lateral growth leads to coalesce and form AlN films with a few sub-grains.

In sample with AlN NL of 100 nm thickness, the topmost GaN layer is observed to grow non-uniformly and this problem is mainly due to the weak nucleation and uniformity of AlN layer. Above the coalesced AlN layer, more AlN nuclei were formed with continued deposition. When thicker AlN of 200 nm (higher growth time) is used, the sub-grains continue to grow while experienced lateral and vertical growth with higher overall lateral growth rates, and coalesced laterally. This significant lateral growth rate results in a pseudo-2-dimensional growth mode of the AlN which results in flat, uniform surface of AlN as can be seen in Figure 4.4(c).

Another factor which improves the surface homogeneity of the grown AlN in the epitaxial structure is high growth temperature that were used in this deposition. High temperature provides sufficient energy which increase the mobility of AlN to fix the misfit in their crystal structure during growth process. Moreover, AlN favours high temperature to grow epitaxially and the high growth temperature successfully accommodate a good epitaxial growth of AlN in the structure. The results differ clearly with the preliminary sample since the 50 nm thickness of AlN produces cloudy surface as compared to several micro-cracks and melt-back spot when the AlN thickness is 20 nm.



Figure 4.4: FESEM cross section images of varied AlN thickness of (a) 50 nm, (b) 100 nm and (c) 200 nm thickness under 100k magnification, respectively.

In order to justify the effect of varying the AlN nucleation layer on the surface roughness and morphological properties of the topmost GaN layer, AFM surface imaging was done on the sample. Table 4.3 shows the 2-dimensional (2D) and 3-dimensional (3D) AFM images and properties of the topmost GaN layer at different AlN NL thickness.

AlN NL thickness (nm)	50	100	150
2-dimensional AFM image (5 × 5 μm ²)			
3-dimensional AFM image (5 × 5 μm ²)			
RMS Roughness (nm)	4.974	2.872	2.470
Peak to valley (nm)	11.028	8.782	7.712

Table 4.3: 2D, 3D images and the properties of topmost GaN layer with variation of AlN NL thickness.

Based on the results in the table above, the RMS roughness and the peak to valley distance of the topmost GaN layer is significantly reduced. The surface of topmost GaN layer becomes more coalescence as the AlN nucleation layer thickness is increased from 50 nm to 100 nm. At thickness of 50 nm, the topmost GaN layer exhibits a small granular surface which contributes to higher surface roughness. Thus, the surface becomes smoother as the thickness of AlN NL increase. The AlN sample coalesce properly during growth and affects the smoothness of the top GaN layer. This effect is probably contributed by low mobility of AlN during growth process. During initial growth phase, AlN slowly forms during growth and slowly coalesce with time. However, it is extremely challenging to achieve smooth GaN on AlN when the thickness of AlN becomes higher.

Luo et al. (2008) concluded that the optimum thickness that is achieved in his sample is around 110 nm and the sample degrades as the AlN thickness is increased above 110 nm. In this research, however, the topmost GaN produce a smoother surface even after the thickness is increased above 110 nm. This is probably due to high growth temperature of AlN of 1000 °C which accommodate the movement of AlN molecules. Since AlN coalesce more properly with the increase in AlN thickness, the peak to valley also slowly reduces which indicates high quality behaviour of AlN. The ability to grow higher thickness of AlN to produce an even better coalesce GaN layer highlights the potential of HT-AlN layer to be the material template for high power applications.
4.4 Nitridation Surface Treatment (NST)

In this chapter, nitridation surface treatment is introduced as another key epitaxial layer on growing non-crack GaN on Si (111) substrate. Thin AlN nucleation layer failed to reduce the melt-back etching issue and therefore a new surface treatment was introduced during deposition process. This chapter will focus on the results for effect of varying the nitridation time towards the structural and morphological properties of the sample. Subsequently, the quality of the sample is further compared with the preliminary sample to highlight the need of nitridation surface treatment in the epitaxy process.

4.4.1 Nitridation Surface Treatment (NST) for GaN Epitaxy on Silicon

In this study, the nitridation surface treatment process was carried out followed by growing a thin AlN nucleation layer and AlN/GaN multi-layer which act as the buffer and strain compensating layer, respectively. The nitridation treatment was done in the metal organic chemical vapor deposition (MOCVD). The nitridation time was varied to three different durations of 40, 220 and 400 seconds in order to optimize the GaN epilayer quality grown on Si(111) substrate. The parameters of the other layer are kept constant as in the preliminary sample. This thesis reported on the SiN_x layer formed during NST process on Si(111) substrate, by which the sample bowing, surface roughness and dislocation density are critically affected.

The NST on the Si(111) substrate before the subsequent growth is identified as a vital step to obtain a high quality of GaN epilayer grown on Si(111) substrate. The surface of the topmost GaN appears specular and exhibit mirror-like properties when the nitridation was carried out at 400 s. No micro crack is observed under naked eyes observation propagating on the topmost GaN layer. Figure 4.5 shows the naked-eye observation of the topmost GaN layer on Si (111) substrate.



Figure 4.5: Naked eye observation of the sample grown with 400 s nitridation time.

4.4.1.1 Morphological Properties

To further study the morphological properties of the topmost GaN in detail, the sample was examined by AFM. It has been reported that the nitridation time affect the surface roughness of the nitridated growth when it was incorporated with the thin AlN nucleation layer and AlN/GaN multi-layer (Nakamura et al., 1993; Jain et al., 2000). Table 4.4 shows the AFM images of GaN/Si surface morphologies with substrate being nitridated at 1000 °C for 400, 220 and 40 seconds incorporated with a thin AlN nucleation layer and AlN/GaN strained-layer superlattice (SLS).

Table 4.4: 3D, 2D images, the rms roughness and the peak to valley value of the topmost GaN layer at different nitridation duration of (a) 400 seconds, (b) 220 seconds and (c) 40 seconds, respectively.

Sample	a) 400 seconds	b) 220 seconds	c) 40 seconds
3-Dimensional Image (5 μm x 5 μm)			
2-Dimensional Image (5 μm x 5 μm)			
RMS Roughness (nm)	1.475	2.153	3.365
Peak to Valley Value (nm)	4.247	7.416	9.846
		2 P	

As it can be seen in Table 4.4, the value of root mean square (RMS) roughness for the top GaN epilayer is decreasing from 3.365 to 1.475 nm as the nitridation time was increased from 40 to 400 s. The AFM images also proved that the top GaN epilayer was found to be more uniform and homogenous compared to the others at 400 s of nitridation time, with smallest grain size and peak to valley value at 4.247 nm. It has been reported widely that a SiN_x layer was formed prior to the NST process on the silicon substrate (Ozturk et al., 2013; Pal & Jacob, 2004). This SiN_x layer can improve the crystal quality of the top GaN epilayer while efficiently prevented the substrate from any oxygen diffusion and silicon gasing process from reacting with the gallium during the GaN growth (Ozturk et al., 2013). Hence, it will oppose the melt-back etching issue (Ishikawa et al., 1998; Ishikawa et al., 1999; Able et al., 2005). The GaN grains gradually coalesced with reduction in cluster size, suggesting the transition in growth mode from three-dimensional towards two-dimensional like growth (Wuu et al., 1999).

A high quality of GaN epilayers also can be produced through restraining the sample bowing from the substrate during the epitaxial growth. It has been reported that the substrate bowing could be compressed by inserting strained-layer superlattice as the strain compensating layer in a particular growth structure (Aida et al., 2011). In this set, we have applied a thin AlN nucleation layer and 40 pairs of AlN/GaN multi-layer to inherit the former publications. Figure 4.6 shows the graph of wafer bowing of the sample against different nitridation time.



Figure 4.6: Graph of wafer bowing (µm) against nitridation time (s).

From the plotted graph, it is observed that from range of 50 to 220 s, the bowing effect on the silicon substrate greatly reduces from 82 μ m to around 55 μ m. This value is expected as it was also been observed by Rowena et.al. (2011). It is found that the bowing of the samples decreased as we increased the nitridation time, in which the lowest bowing of 51.99 μ m was recorded at 400 s of nitridation time. It is crucial to mention that the compressive stress generated in the front-side surface of Si(111) substrate after growing the GaN layer is greatly influenced by SiN_x layer formed at 400 s of nitridation time. SiN_x formed during nitridation process act as stress compensating layer during cooling process as mentioned in several works (Hiramatsu et al., 1993; Selvaraj et al., 2009; Dadgar et al., 2011; Dadgar et al., 2007). This layer counteracts the bowing effect suffers during cooling process in Si (111) growth, which in turn reduce the bowing values as illustrated in Figure 4.6. Therefore, the exposure time of nitridation treatment on Si (111) surface also significantly affects the surface quality and bowing for the growth of top GaN epilayers.

In order to confirm the morphological structure on the topmost GaN layer, FESEM surface scanning and cross section imaging was done on the sample to determine the smoothness of GaN layer. Figure 4.7 shows the result of surface and cross section FESEM images on the topmost GaN layer.

The surface scanning done under 1000 magnification, proves that, no cracks and pits have been detected for the top GaN epilayer growth at 400 s of nitridation time. The cross-sectional FESEM image of topmost GaN layer grown at 400 s of nitridation time also shows a smooth conformal layer structure as illustrated in Figure 4.7(d). Hence, the SiN_x layer formed at 400 s of nitridation time is efficiently blocking the Si/Al and Si/Ga inter-diffusion during the III-nitrides growth (Uen et al., 2005).



Figure 4.7: The surface scanning images of GaN grown on Si(111) substrate at (a) 400 s, (b) 220 s and (c) 40 s of nitridation time and (d) the cross-sectional image of the GaN epitaxial growth on silicon (111) substrate at 400 s of nitridation time.

This results validated the NST process is crucial in order to sustain the tensile strain on each heteroepitaxy layer. Thus, it can indirectly diminish the defect that commonly occurred during the growth of GaN on silicon(111) substrate (Dadgar et al., 2000). These results have concluded that a high quality of topmost GaN epilayer with a smooth and fine epitaxial surface grown on Si(111) substrate is successfully achieved after the NST process for 400 s nitridation time. In terms of generation of crack, the absence of meltback etching from efficient nitridation surface treatment prevents the formation of crack in the sample as illustrated in Figure 4.7(a).

4.4.1.2 Structural Properties

Since the morphological results confirmed all the observations logically, the structural quality of the topmost GaN layer have been observed using x-ray rocking curve (XRC) measurement. The XRC (0002) analysis was performed to study the screw dislocation while the XRC ($10\overline{1}2$) for the edge and mixed dislocation that occurred in the top GaN epilayer (Arslan et al., 2009; Metzger et al., 1998). The graph obtained for both analyses are presented in Figure 4.8(a) and (b).

The graph shows that the FWHM value for both analyses become narrower as the nitridation time is increased. It can also be observed that the sample at 400 s of nitridation time exhibits the lowest FWHM with 1126 arcsec for (0002) and 2012 arcsec for $(10\bar{1}2)$ measurement. The reductions of FWHM value as the nitridation time increased indicates the reduction of dislocation density in the topmost GaN epilayer (Arslan et al., 2009; Metzger et al., 1998). Si usually outgases during growth and produce dislocation sites as Si reacts with Ga to produce gallium silicide. Nitridation surface treatment provides an additional barrier which reduce the formation of gallium silicide, thus reducing the dislocation density inside the sample. It can be concluded that NST technique under 400s duration is effective towards blocking Si/Al and Si/Ga inter-diffusion during the III-nitrides growth. This leads toward a perfect growth of AlN/GaN strained-layer superlattice (SLS) as shown in Figure 4.7(d).



Figure 4.8: The XRC measurement of (a) (0002) and (b) $(10\overline{1}2)$ scan of samples deposited at different nitridation time.

The propagation of screw and edge, mixed dislocation has significantly been improved by multi-layer area (Hageman et al., 2001). Thus, this finding has supported the previous result whereby a high quality of topmost GaN epilayer grown on Si(111) substrate has been well produced. However, it needs to be mentioned that the value of FWHM can further be decreased if the thickness of top GaN epilayer is increase as the incident X-ray will penetrate into the sample and only identifying the GaN lattice instead of other materials lattice from bottom layer. Hence, these results are comparable with other publication, whereby the FWHM value was around 500-600 arcsec for top GaN epilayer at thickness of 2.2 µm (Krost et al., 2003; Dadgar et al., 2007). This also explains why $(10\overline{1}2)$ peak is weakly comparable although the difference in duration of nitridation time is quite large. Since the morphological and structural properties of the nitridated sample already provide a promising properties without any cracking appearance on the sample, the quantitative analysis on the sample was finally done by calculating the dislocation density of all samples. The aforementioned Equation 4.2 and 4.3 was used to determine the dislocation density on the topmost GaN layer. Table 4.5 shows the screw, edge and mixed as well as the total dislocation density inside the sample for GaN epitaxy being nitridated at three different nitridation time of 40, 220 and 400 s. In order to analyse the trend of reduction more clearly, graph of dislocation density against nitridation time is plotted as shown in Figure 4.9.

Table 4.5: Screw, edge and mixed, and total dislocation density for sample nitridated at different nitridation time.

Nitridation Time (s)	40	220	400
Screw dislocation density (D_{screw}) (×10 ⁹ cm ⁻²)	7.48	1.41	1.23
Edge and mixed dislocation density ($D_{edge and mixed}$) (×10 ¹⁰ cm ⁻²)	7.30	1.14	1.04
Total dislocation density (D_{total}) (×10 ¹⁰ cm ⁻²)	8.05	1.28	1.16



Figure 4.9: The screw and edge, mixed dislocation density of samples deposited at different nitridation time.

From Figure 4.9, it can be distinctly observed that the lowest dislocation density was achieved at 400s of nitridation time. The result is expected due to several supportive reasons such as the specular, mirror-like surface of the sample, reduction in AFM roughness and bowing effect possessed by the sample, crack-free surface as seen under microscope and lastly, the reduction in FWHM of the sample being nitridated at 400 s. Based on this basis, the necessity of nitridation surface treatment process to achieve mirror-like surface GaN on Si (111) epitaxy is properly highlighted and deduced as one of the key parameter to achieve high quality GaN on Si (111) substrate.

4.5 AIN/GaN Strained-Layer Superlattice (SLS)

In this chapter, AlN/GaN strained-layer superlattice (SLS) growth will be discussed as another key parameter to grow non-crack GaN on Si (111) substrates. Chapter 4.5.1 will briefly introduce the necessity of investigating the influence of AlN/GaN SLS for GaN epitaxy on Si (111) substrates. The effect of manipulating the AlN/GaN SLS layer parameter will be discussed in Chapter 4.5.2.

4.5.1 AIN/GaN SLS for Crack-free GaN Surface

While nitridation surface treatment (NST) acts as an epitaxial passivation layer for the growth of polycrystalline GaSi during GaN growth as can be seen in previous chapter, AlN/GaN SLS serves as dislocation buffer layer and functioned to reduce the higher bowing effect of thicker GaN on Si (111). Driven by the motivation to achieve thicker crack-free GaN on Si (111), the AlN/GaN SLS effect as dislocation filtering layer will be described in detail throughout this chapter. The ability of AlN/GaN SLS in assisting crack-free epitaxial GaN layer will also be discussed in this chapter. The large lattice and thermal mismatch of AlN and GaN will create edge dislocation inside the lattice due to incomplete and missing atomic arrangement inside the layer.

The conversion factor from AlN lattice to GaN lattice will usually create a gap in between the lattice matching and introduce uncontrolled tensile stress on the GaN epilayer. The effect increases towards thicker GaN layer until certain specific thickness denoted as critical thickness where such effects generate cracking of GaN layer on Si due to incapability of AlN to compensate higher generated tensile stress of GaN. It is well known that dislocation and cracks will also deteriorates the device quality and generally induce unwanted thermal accumulation inside the sample. Owing to such reason, a strain compensating technology involving the usage of AlN/GaN SLS have been introduced to compensate the strain and lead towards avoiding crack issue on the sample. In an effort to properly investigate the effect of AlN/GaN SLS layer towards diminishing crack issues on thicker GaN, the AlN/GaN SLS were grown at 4 different number of pairs while maintaining the parameter of other layers.

4.5.2 Effect of Varying the Aluminium Nitride/Gallium Nitride (AlN/GaN) Strained-layer Superlattice (SLS) Pairs

Four different growth have been done to investigate the effect of AlN/GaN strainedlayer superlattice (SLS) towards achieving crack-free GaN on Si (111) substrates by varying the number of AlN/GaN SLS pairs to 20, 40, 60 and 80 pairs. The efficiency of AlN/GaN multilayer as dislocation filtering and defect annihilating layer to provide high quality GaN epilayer is established by observing the quality of the topmost GaN layer.

4.5.2.1 Morphological Properties

In this work, to study the effect of varying AlN/GaN strain-layer superlattice (SLS) periods on the surface quality of the GaN epitaxial layer, the sample was examined by AFM. Table 4.6 shows the AFM images and the morphological properties in terms of root mean square (RMS) roughness and peak-to-valley value of GaN deposited on top of AlN/GaN SLS structure with varying periods of 20, 40, 60 and 80 pairs.

As stated in Table 4.6, the value of RMS roughness is decreasing as the number of AlN/GaN SLS periods in the GaN structure increases from 20 to 60 pairs. At 80 periods of AlN/GaN SLS, the RMS value slightly increase suggesting some sort of surface degradation occurring in top GaN layer. Lowest peak-to-valley value was achieved for

sample with 60 periods of AlN/GaN SLS before a sudden increase of peak-to-valley in sample at 80 AlN/GaN SLS. The coalescence process of AlN/GaN SLS is the vital condition towards achieving crack-free topmost GaN layer. While sample with 60 periods of AlN/GaN SLS effectively reduce the roughness of topmost GaN layer, sample at 80 periods of AlN/GaN SLS experience a deterioration in terms of roughness and peak to valley value.

Valcheva et al. (2003) relates this behaviour towards the alternating tensile/compressive strain within each period due to lattice mismatch between AlN and GaN layers. The overall composition of AlN in the AlN/GaN SLS might also induced the formation of island-like structure on the topmost GaN layer. It is deduced that for 80 periods of AlN/GaN SLS the 3D growth effect dominates the 2D growth which explains the increase in peak to valley value from 4.8 nm to 7.9 nm. At the same time, the roughness of GaN/Si also increases from 1.617 nm to 2.887 nm.

No. of AIN/GaN SLS pairs	3 Dimensional (3D) Image	Average Roughness (RMS) (nm)	Peak to Valley (nm)
20		1.900	5.083
	00		0
40		1.674	5.025
60	m 75 6 7 7 7 7 7 7 7 7 7 7 7 7 7	1.617	4.781
80	m 19 10 10 10 10 10 10 10 10 10 10	2.887	7.953

Table 4.6: Average	roughness and	peak to	valley ((P-V)	of grown	sample.

While bowing have been detected as one of the crucial parameter which controls the cracking issues in GaN epilayer, an increase in the number of AlN/GaN SLS periods from 20 to 40 results in a decrease in bowing effect of the sample as can be seen in Figure 4.10. However, an increment in bowing value was obtained from 65 μ m to 100 μ m as the periods of AlN/GaN SLS were increased from 40 to 60 pairs. Despite the increase in bowing value, a crack-free top GaN layer was successfully achieved for sample of 60 periods of AlN/GaN SLS.

The result obtained was against several reports which relates formation of high quality GaN epilayers with lower bowing parameter during epitaxial growth (Hiramatsu et al., 1993; Dadgar et al., 2011; Cheng et al., 2011; Sakai et al., 2004). The possible explanation to this result lies on the epitaxial engineering behind the introduction of AlN/GaN superlattice itself. During epitaxial growth, a large stress is induced due to large lattice mismatch between AIN buffer layer and Si. The initial AIN nucleation layer usually comprises of high dislocation density due to strain relaxation in the film. (Ubukata et al., 2007). Introduction of AIN in SLS induces compressive stress to the subsequent period of AlN/GaN SLS which counterbalances both the growth-induced tensile stress and the thermally-induced tensile strain in SLS during cooling process.

The doping of Si in GaN is responsible in introduction of tensile stress in those layer, although the substitution of Si for Ga only causes negligible changes in the lattice constant (Cheng et al.,2011). The tensile increase explained the finding of crack in sample inherited with 40 AlN/GaN SLS although the bowing of the overall structure was slightly reduced as compared to 20 AlN/GaN SLS. Since the growth have been done under slight doping of Si throughout the whole layer to increase the carrier mobility of buffer layer, it is found that unintentionally Si-doping also increase the tensile effect on the topmost GaN layer (Manning et al., 2010). Therefore, this clearly explaining the crack-free GaN obtained despite that quite large bowing value as compared to many publications. It is

therefore concluded that under such Si doping, 60 pairs of ALN/GaN SLS was sufficient to act as an effective dislocation barrier to produce crack-free GaN. Although the bowing increment can be related to the total Al composition in the structure, much works shall be done to support such basis.



Figure 4.10: Bowing against total thickness of sample.

To further confirm our observation, the samples were characterized using FESEM for the top-view and the cross section images of our structure. Figure 4.11(a), (b), (c) and (d) refer to the top-view image of FESEM under 10K magnification. The image shows absence of cracks for the top-GaN epilayer growth at 60 periods of AlN/GaN SLS. Several small pits were still present as indicated by the small arrow in Fig 4.11(c). However, such pits did not contributes in the formation of cracks on the sample. The cross-sectional image also shows fine, abrupt structure of AlN/GaN SLS at 60 periods as illustrated in FESEM surface depicted by Figure 4.11(c). The results justified the crackfree GaN that were obtained in the sample, thus relates the necessity of getting a fine SLS structure which can effectively act as dislocation filtering layer. Astonishingly, the crack reappears in sample deposited at 80 periods of AlN/GaN SLS. The above observation supports the previous deduction that with higher aluminium to overall AlN/GaN structure content, the surface quality deteriorates back and crack have been generated back. With respect to AFM images, a clear outline was given that to achieve a high quality crack free GaN epilayer with smooth and fine surface of topmost GaN, the AlN/GaN SLS should be abrupt and fine with controlled, fixed thickness to sustain the strain-stress counterbalance generated in AlN/Si interface during AlN/GaN SLS growth.

Based on Figure 4.12(b), the AlN/GaN SLS interface is fine and abruptly formed with uniform thickness. Thus, it is later concluded that the only reason in the increase of bowing and deterioration of topmost GaN quality on sample deposited at 80 pairs of AlN/GaN SLS was mainly due to the Al content in the overall structure. While for sample deposited with 60 pairs of AlN/GaN SLS, the AlN introduced in the SLS structure perfectly counterbalanced the tensile effect by inducing compressive stress in the structure during cooling process to produce crack-free GaN on Si(111) substrates (Cao et al., 2016).



Figure 4.11: FESEM surface of sample with different SLS pairs of (a) 20 pairs, (b) 40 pairs, (c) 60 pairs and (d) 80 pairs viewed under 10K magnification.



Figure 4.12: (a) Cross section image of overall structure under 100k magnification, and (b) Cross section image of multi-layer thickness under 200k magnification, respectively.

Based on Figure 4.12(b), the AlN/GaN SLS thickness was uniformly grown with a precise thickness of 13.11 nm for GaN layer and 10.20 nm for AlN layer. Such thickness contributed to the GaN and AlN growth rate of 0.49 nm/s and 0.70 nm/s, respectively.

4.5.2.2 Structural Properties

While the images of FESEM and AFM have already provide such understanding, XRC analysis was carried out to further investigate the influence of varying the number of periods of AlN/GaN SLS towards the structural properties of GaN grown on Si (111) substrates. Two kinds of in-plane characterizations was done using XRC analysis on (0002) and ($10\overline{1}2$) plane for the edge and mixed dislocation that happened in the top GaN epilayer. The graph for both analyses are presented in Figure 4.13(a) and Figure 4.13(b). The graph shows the narrowest FWHM value for sample deposited with 60 periods of AlN/GaN SLS. Further increase in the number of periods of AlN/GaN SLS shows an increase in both edge and mixed dislocation of the sample.

The reductions of FWHM value as the AIN/GaN SLS were increased, indicates the reduction in dislocation density in the top GaN epilayer. Such results clearly shows the function of AIN/GaN SLS to reduce and compensate the propagation of the screw, edge and mixed dislocation in the sample (Hageman et al., 2001). However, it is compulsory to mention that the value of FWHM can be further reduced if we increase the thickness of top GaN epilayer since the incident x-ray will only detect the dislocation in the top GaN epilayer instead of other layers. It is convinced that the FWHM that were obtained comprises of the total dislocation in the AIN/GaN SLS and the top-GaN epilayer itself. Several works also have reported that the threading dislocation might penetrates the AIN/GaN SLS up to several hundred nanometres before completely terminated depending on the composition and type of SLS materials. Hence, these results are comparable with other publication, by which the FWHM value was around 500 to 600 arcsec for top GaN epilayer at thickness of 2.2 μ m (Dadgar et al., 2003; Krost et al., 2003).



Figure 4.13 (a) (0002) and (b) ($10\overline{1}2$) XRC scan for all samples deposited at different number of AlN/GaN SLS pairs.

While morphological and structural analysis already suggested 60 pairs of AlN/GaN SLS as optimum periods to effectively reduce the dislocation density based on FWHM result, numerical calculations have been made to confirm and obtain the figurative value. The aforementioned Equations 4.2 and 4.3 was used to determine the dislocation density on the topmost GaN layer. Table 4.7 shows the screw, edge and mixed, and the total dislocation density value for the samples deposited at different AlN/GaN SLS periods of 20, 40, 60 and 80 pairs. In order to analyse the trend of reduction more clearly, graph of dislocation density for screw and edge, mixed dislocation density against number of AlN/GaN SLS pairs is plotted as shown in Figure 4.14.

Table 4.7: Screw, edge and mixed, and total dislocation density for sample deposited at different number of AlN/GaN SLS pairs.

No. of AIN/GaN SLS pairs	20	40	60	80
Screw dislocation density (D_{screw}) (×10 ⁹ cm ⁻²)	12.60	2.87	2.45	2.70
Edge and mixed dislocation density $(D_{edge and mixed}) (\times 10^{10} \text{ cm}^{-2})$	11.70	1.54	1.19	1.32
Total dislocation density (D_{total}) (×10 ¹⁰ cm ⁻²)	13.0	1.83	1.44	1.59



Figure 4.14: The screw and edge, mixed dislocation density of samples deposited at different number of AlN/GaN SLS pairs.

From Figure 4.14, it can be clearly seen that the lowest screw and edge, mixed dislocation was achieved using epitaxial technology involving growth with 60 pairs of AlN/GaN SLS structure. The result is expected due to several supportive reasons such as the reduction in AFM roughness and bowing effect possessed by the sample, crack-free surface as seen under microscope and lastly, the reduction in FWHM of the sample being grown using 60 pairs of AlN/GaN SLS structure.

Based on this basis, the effect of using AlN/GaN SLS to efficiently diminishing the crack issues by manipulation of strain-stress interaction in between the heteroepitaxial layers for GaN on Si (111) substrates have been successfully investigated. Thus, it is concluded that 60 pairs of AlN/GaN SLS technology is the optimum parameter to proficiently achieve 500 nm crack-free GaN epitaxy on Si(111) substrates provided that the overall layer were slightly doped with Si and achieve a thickness ratio for AlN: GaN that is approximately 10 nm: 13 nm.

CHAPTER 5: CONCLUSION

5.1 Introduction

This chapter will summarizes all the results and highlights several discussions that have been stated in Chapter 4. The crucial explanation and significant results towards the conclusion of this thesis will be properly arranged and presented in a systematic manner. The contribution in terms of knowledge and understanding the crack-free growth of GaN on Si (111) substrates will be emphasized. The objectives of the thesis will be properly answered as to indicate the progression in epitaxial technology that have been fully understood by the author. Chapter 5.2 will conclude this work and the current understanding that the author have while Chapter 5.3 will outline the potential future work to preserve the author's motivation towards achieving high quality epitaxial GaN growth on Si (111) substrates.

5.2 Conclusion

Throughout this whole work, a homogeneous, high temperature aluminium nitride (HT-AlN) nucleation layer (NL) have been successfully grown on silicon (111) substrate. The sample is specular at ALN NL thickness of 200 nm. AFM surface imaging provides a RMS surface roughness of 2.470 nm and peak-to-valley value of 7.712 nm. From the homogeneity test, high temperature AlN (HT-AlN) NL was successfully grown on silicon (111) substrate with better HT-AlN NL quality at higher thickness of 200nm. Although preliminary optimization on the AlN thickness shows positive trend towards higher thickness of nucleation layer, in term of device performance, lower AlN NL thickness dictates favourable result with higher device conductivity.

Driven towards this goal, enhanced epitaxial technology involving the usage of nitridation and AlN/GaN strained-layer superlattice (SLS) has been employed to

compensate thinner AlN NL properties towards achieving high quality crack-free GaN epitaxy on Si (111) substrate.

Subsequently, the effect of varying the nitridation surface treatment (NST) time with the quality of topmost GaN layer have been successfully investigated. The best topmost GaN quality was achieved at 400s with specular Si surface as seen by bare eyes. Further characterization on AFM reveals the lowest RMS roughness of 1.475 nm and peak-to-valley value of 4.247 nm. With an increment in NST time, lower bowing effect was achieved on the sample with the lowest one recorded at 51.99 μ m. FESEM images reveal a crack-free 500 nm GaN surface deposited at NST of 400s was achieved when being characterized using FESEM which confirmed our objective. Lowest FWHM was achieved at 1126 and 2012 arcsec for in-plane characterization at (002) and (102), respectively. Numerical calculation displays lowest dislocation density of 1.23 × 10⁹ and 1.04 × 10¹⁰ cm⁻² for screw and edge, mixed dislocation density.

Next, an optimum 60 pairs of AIN/GaN strained-layer superlattice (SLS) was employed to achieve a 1 μ m crack-free GaN growth on is (111) substrate. The lowest RMS roughness and a peak-to-valley value of 1.617 nm and 4.781 nm, respectively was achieved with fine, abrupt SLS structure as depicted in FESEM cross section images. The AIN/GaN SLS thickness was uniformly grown with a precise thickness of 13.11 nm for GaN layer and 10.20 nm for AIN layer. Such thickness contributed to the GaN and AIN growth rate of 0.49 nm/s and 0.70 nm/s, respectively. XRC analysis produces the lowest FWHM of 1103 and 1497 for (002) and (102) in-plane characterization, respectively. In addition, numerical calculation for screw and edge, mixed dislocation shows the lowest value at 2.45 × 10⁹ and 1.19 × 10¹⁰, respectively.

Thus, it is concluded that 60 pairs of AlN/GaN SLS technology is the optimum parameter to proficiently achieve 1µm crack-free GaN epitaxy on Si(111) substrates provided that the overall layer were slightly doped with Si and achieve a thickness ratio

for AlN: GaN that is approximately 10 nm:13 nm. Therefore, a crack-free GaN layer have been successfully grown on silicon (111) substrates.

5.3 Suggested Potential Future Works

Due to the achievement throughout this thesis, several potential future works can be highlighted to further understand the behavioural change of NST and SLS epitaxial technology for GaN growth on Si (111) substrates. The potential future works as suggested are:

- 1. Structural and morphological optimization of AlN/GaN SLS thickness to understand the effect of changing Al composition towards the overall SLS structure.
- 2. Optimization of Si-doped AlN/GaN SLS to achieve smoother and better quality of topmost GaN layer.
- 3. LED epitaxy optimization on Si (111) substrate due to cheaper substrate value and higher potential of silicon to be integrated with current semiconductor technology.

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LIST OF PUBLICATION AND PAPER PRESENTED

Publication

 Rahman, M. N. A., Yusuf, Y., Mansor, M., & Shuhaimi, A. (2016). Effect of nitridation surface treatment on silicon (111) substrate for the growth of high quality single-crystalline GaN hetero-epitaxy layer by MOCVD. *Applied Surface Science*, 362, 572-576. [IF : 3.15]

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Effect of nitridation surface treatment on silicon (1 1 1) substrate for the growth of high quality single-crystalline GaN hetero-epitaxy layer by MOCVD



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A single-crystalline with high quality of gallium nitride epilayers was grown on silicon (111) substrate by metal organic chemical vapor deposition. The process of nitridation surface treatment was accomplished on silicon (111) substrate by flowing the ammonia gaseous. Then, it was followed by a thin aluminum nitride nucleation layer, aluminum nitride/gallium nitride multi-layer and a thick gallium nitride epilayer. The influence of in situ nitridation surface treatment on the crystallinity quality of gallium nitride epilayers was studied by varying the nitridation times at 40, 220 and 400s, respectively. It was shown that the nitridation times greatly affect the structural properties of the grown top gallium nitride epilayer on silicon (111) substrate. In the (0002) and (10 $\bar{1}2$) X-ray rocking curve analysis, a narrower value of full width at half-maximum has been obtained as the nitridation time increased. This is signifying the reduction of dislocation density in the gallium nitride epilayer. This result was supported by the value of bowing and root mean square roughness measured by surface profilometer and atomic force microscopy. Furthermore, a crack-free gallium nitride surface with an abrupt cross-sectional structure that observed using field effect scanning electron microscopy was also been obtained. The phi-scan curve of asymmetric gallium nitride epilayer ENA with the top gallium nitride epilayer exhibited a single-crystalline structure.

1. Introduction

Silicon (111) substrate

Keywords: MOCVD

Nitridation

Crack-free GaN

The III-nitride materials such as gallium nitride (GaN) have become one of the most favorable materials in the fabrication of optoelectronic devices. This is owning to a great mechanical and optical properties like high thermal conductivity together with high melting points, high hardness, low dielectric properties and a wide band gap energy which covers the spectrum in the range of visible to the near ultraviolet region [1].

Currently, silicon (Si) substrate is considered a relatively capable substrate for GaN epitaxy since it is low cost, available in large scale and conducting in nature [2]. However, it has been understandable that to grow a high quality of GaN epilayer on Si substrates is considered difficult due to their large lattice mismatch (16%), chemical dissimilarity and huge thermal mismatch (54%) which resulting a high level of in-plane stress. This leads to the generation of defects in the growth of GaN epilayer [3]. The poor nucleation properties of GaN epilayer [4]. It has been reported that a temperature around

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http://dx.doi.org/10.1016/j.apsusc.2015.10.226 0169-4332/© 2015 Elsevier B.V. All rights reserved. 1200K with hydrogen (H₂) ambiance, out-gases silicon formed a Gallium Silicide (GaSi₃) during the GaN growth. This led to hinder the formation of a homogenous GaN epilayers grown on Si substrate [2]. Therefore; many efforts have continuously been introduced to overcome these issues.

Recently, remarkable work has been reported about the growth of a single-crystalline GaN on Si substrate. Where, it has been done by manipulating the buffer layer thickness, growth temperature, compound concentration and the ammonia (NH₃) flow rate. Wu-Yih Uen et al. [4] studied the influence of in situ substrate nitridation temperature on the GaN crystalline quality where the nitridation process was done at 750, 950 and 1120 °C, respectively. They reported that the applied temperature during nitridation process greatly influences the surface morphology and photoluminescence (PL) spectra of the top GaN epilayer grown on the formed silicon nitride (SiN_x) layer. Dong-Sing Wuu et al. [7] showed that in order to produce a mirror-like GaN layer could be induced at longer annealing period and caused a smaller grain size. They also reported that the NH₃ flow rate is contributed in the homogeneity of the growth GaN epilayer on Si substrate. Engin Arslan et al. [5]